

Leon Valley Baptist Church Recreational Center Design II - 2025

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Subject: Final Report for the development of an indoor Recreational Center for Leon Valley Baptist Church

Dear City of San Antonio,

Lone Star Engineering has been commissioned to design a one-story indoor recreational center for Leon Valley Baptist Church, located on Grissom Road near Bandera Road in San Antonio, Texas. The planned facility will include an indoor basketball court, multi-use/pickleball rooms, lobby, restrooms, offices, and storage areas, complemented by outdoor amenities such as a sand volleyball pit and a tennis court.

This report provides the documentation necessary for the successful planning and development of the project. Our vision is to create a functional and welcoming recreational space that promotes community engagement, supports healthy lifestyles, and enhances the ministry's outreach.

Lone Star Engineering is committed to upholding the highest professional, ethical, and legal standards throughout the design and development process. We place the utmost importance on safety, integrity, and longevity, ensuring the facility serves both current and future generations of the church and its surrounding community.

We pledge to apply our complete expertise and dedication to deliver a safe, compliant, and enduring recreational center that reflects the values and mission of Leon Valley Baptist Church.

Sincerely,

Lone Star Engineering



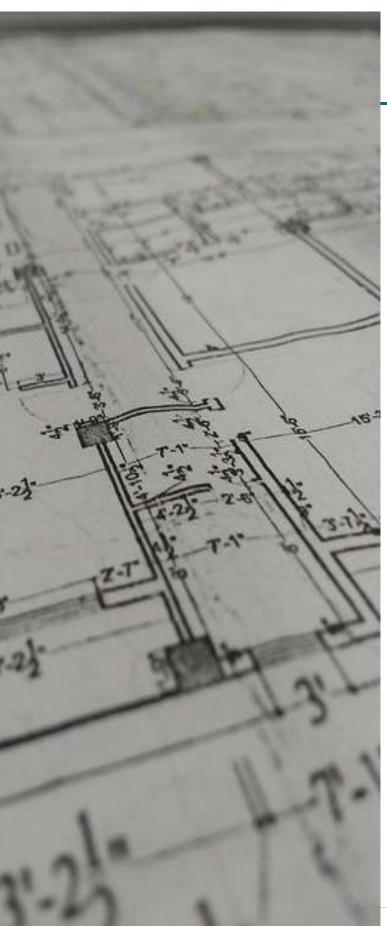


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Project Scope

Leon Valley Baptist Church has acquired 17.434 acres of land directly behind its existing facilities to develop a new indoor recreational center. The proposed building will measure 150 feet by 175 feet, covering approximately 26,250 square feet, not including the planned outdoor amenities. The facility will feature an indoor basketball court, multi-use rooms for activities such as pickleball, a lobby, restrooms, offices, and storage areas, providing flexible, functional space for church members and the broader community, as illustrated in Figure 1.

Outdoor features will include a sand volleyball pit and a tennis court, enhancing on-site recreational options. The project's scope encompasses comprehensive site planning, architectural and structural design, grading and drainage considerations, utility connections, and compliance with all applicable codes and permitting requirements to ensure a safe, sustainable, and durable facility.

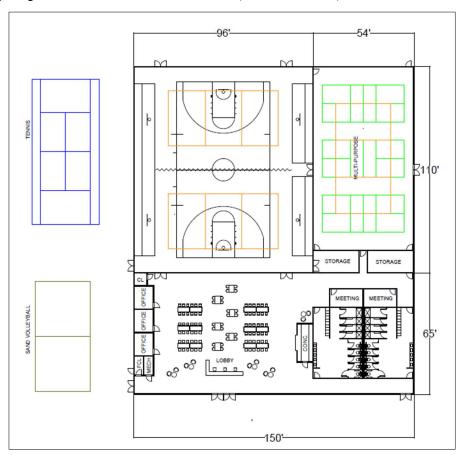


Figure 1: Proposed Floor Plan



Land Development & Environmental

Our project will be developed behind the Leon Valley Baptist Church, 7980 Grissom Road, San Antonio, Texas. This means that although it's named after Leon Valley, the property is within the City of San Antonio and is subject to its codes.

Zoning

The property is currently zoned R-6, with surrounding R-6 and RM-6 zones, both residential and mixed residential. The property does not have a cultural or historic district designation, and it is not a conditional district. Per sec 35-311 of the SA UDC, a recreational facility addition for a church is allowed.

Plat

The church currently owns the property and is commissioning the project on the 17.434-acre plot. There are no lots or subdivisions, and since we are not fronting a major street, it is considered a major plat.

Tree Preservation Plan

The property has eight (8) heritage trees, all of which will be preserved. To ensure the root protection zone is not disturbed during construction, a temporary chain link fence will be erected around the heritage trees. For the project, a building permit and a tree removal permit will be needed since some trees will be removed. The tree survey will be done with the Stand delineation method per COSA's UDC, which has requirements of 6" Pixels and a 1" = 400' Scale. The program used is ArcView, which is allowed per the SA UDC. Tree preservation must be done at 35% non-heritage and 100% heritage for the property area not in the floodplain. For the floodplain, 80% of non-heritage trees must be preserved, and 100% of heritage trees must be preserved. Since most of the trees are on the south side of the property, the final tree canopy requirement of 38% for a residential area will be easily met.

Habitat Compliance Form

A habitat compliance form must be submitted along with the tree preservation plan. The property is not within Karst zones 1 or 2. According to the Fish and Wildlife Services, our property is in Karst zone 3b, which has a low probability of encountering karst invertebrate species, and we are not within any of the seven listed species designated critical habitats. According to the Texas Parks and Wildlife Department's guidance manual, the property is not within the critical habitat for the Golden Cheeked Warbler, and it has a low probability of being a potential habitat because high-density residential areas surround us. The property does not contain Ash Juniper trees in conjunction with the oak species listed and the canopy covers listed. The form is in Appendix A.



National Park Service (NPS)

Cathedral Rock Park, which lies next to the property, is not managed by the NPS. There are no other nearby parks or trails, so we will not have to worry about NPS restrictions.

The National Environmental Protection Act 1970

It has constraints associated with property around federal land or properties receiving federal funding, neither of which will apply to the property we are working on. Since there will be no modifications to bodies of water (Culebra Creek, which runs along the bottom of the property), we will not need to coordinate with the DOD/US Army Corps of Engineers.

The Clean Water Act 1972

Section 404 has constraints on dredged material and fill material that may be discharged into bodies of water. During construction, since our project is larger than 1 acre, we will need a General Permit to Discharge under the Texas Pollutant Discharge Elimination System for any fill material or other debris generated. This will require a Storm Water Pollution Prevention Plan, prepared in accordance with TCEQ and COSA guidelines.

The Endangered Species Act 1973

Texas has 120 endangered and threatened species with designated critical habitats, and our property is not located in any of them. While 11 species may have a possible range within the property, none were observed during a site visit. These include seven karst species (arachnids and beetles), two birds (Piping plover and Rufa Red Knot), a crustacean (Peck's cave amphipod), and a plant (Texas wild rice). Suppose any of these species is found during construction. In that case, a Conservation Benefit Agreement (CBA) can be arranged with the Fish and Wildlife Service to protect or manage them, facilitating construction and preventing harm.

The Migratory Bird Treaty Act 1918

The purpose of this initiative is to protect the 1,106 bird species listed, preventing them from being harmed or exploited. The property is located within the range of two threatened species: the Piping Plover and the Rufa Red Knot. While a site visit found no signs of these birds, their migratory nature necessitates vigilance during the year-long construction process. If encountered, the MBTA gives anyone the authority to capture and release them nearby, humanely. For removal from the property, coordination with the US Fish and



Wildlife Service is required, and the primary method will be donation to an authorized recipient within the state, ensuring that no species is held for more than 7 days unless otherwise specified.

Storm Water Pollution Prevention Plan (SWPPP)

The Leon Valley Baptist Church Recreational facility will be monitored in accordance with TCEQ TPDES guidelines during its construction. It is a 26.25 sq-ft floor plan on a 17.434-acre property that connects to Grissom Road via Leon Valley Baptist. The Clean Water Act of 1972 maintains water quality in rivers and streams and establishes rules and mitigation measures. The Water Quality Act, enacted in 1987, governs this SWPPP and stormwater runoff management during construction. The property is not within COSA's mandatory detention zone, Edwards Aquifers' recharge or contributing zones, and currently does not have any negative impact on existing drainage or flow paths. Because of the top-down elevation in which the height decreases from north to south. Stormwater currently drains into Culebra Creek with sheet flow throughout the property.

Drainage

A detention pond will be in the southwest portion of the property to retain stormwater and prevent any negative impact on the surrounding area, including Leon Creek, which borders the west and south sides of the property. The property has been divided into six distinct areas, all designed to promote sheet flow.

The detention pond will incorporate swales along its western, eastern, and southeastern borders to direct runoff into the pond. These swales will be constructed with 4 inches of topsoil and will be covered with sod to provide permanent erosion control. Additionally, temporary erosion control measures, such as silt fencing, will be installed during construction to prevent construction materials from being washed away during storms.

Select fill will be used for the detention pond berm, and the overall construction process for the property will primarily involve select fill, with minimal excavation required. The detention pond is also designed with an emergency outlet to handle historic rainfall events, which will direct excess water southward into the southwest quadrant of the property, eventually flowing into Culebra Creek.

Potential Contamination

The primary area at risk of contamination will be the parking lot, where vehicles may be parked and leaking fluids or importing mud, which can be washed away during rainfall events.



As noted, select fill will be utilized, so a General Permit to Discharge under the Texas Pollutant Discharge Elimination System will be obtained. This Stormwater Pollution Prevention Plan (SWPPP) will be part of that process.

BMP

The primary method for addressing stormwater contaminants will be through passive means, utilizing a detention pond and the swales that channel water into it. During the first week after installing sod in the swales, a temporary concentrated irrigation system will be implemented to promote growth and rooting of the sod. Additionally, no vehicles will be allowed to park on the property for more than one week. This restriction will be enforced in collaboration with the church and, if necessary, local law enforcement.

Facility monitoring plans

An inspector will be hired to conduct weekly inspections of the property to ensure BMPs are met and that no additional stormwater pollutants are discharged during construction. A Construction Storm Water Pollution Prevention Plan Field Inspection and Maintenance Report will be conducted every week, regardless of rainfall. These documents will have to be signed, and an archive will be kept. A year after construction is completed, an additional inspection will be conducted, followed by another a year later, to ensure that the facilities' BMPs are being implemented, and a record of their effectiveness will be maintained.

Implementation

The detention pond and swales will be noted as implemented only after they are fully constructed and operating. The temporary silt fencing will be implemented immediately at the beginning of construction. Sod installation will be done at the end of the detention pond, and swale configuration construction and irrigation will be done for the entire week after. A licensed irrigator will be contracted to do the irrigation. The two annual inspections will be conducted the year after construction is completed and the year following.

An example of a SWPPP is provided in Appendix B.



Geotechnical

The results of the Geotechnical Engineering Study for the proposed Leon Valley Baptist Church-Recreational Center, located in San Antonio, Texas, are presented in this report.

The primary objective of this geotechnical study was to conduct subsurface exploration and laboratory testing to determine the soil and groundwater engineering properties at the site.

The exploration involved drilling to a depth of 15 feet using hollow-stem augers, along with Standard Penetration Tests (SPTs) conducted at regular intervals to measure soil resistance. Soil samples were collected using a split-spoon sampler, ensuring their integrity during transportation to the laboratory for classification and analysis. Figure 2 illustrates the site's boring locations.

The laboratory tests included assessing natural moisture content, performing Atterberg limit tests (liquid limit [LL], plastic limit [PL], and plasticity index [PI]), and conducting grain-size analysis. These analyses were crucial for evaluating in situ strength indicators (N values) and classifying soil index properties as illustrated in Appendix C.

Additionally, groundwater levels were monitored during and after drilling to assess potential water-table conditions. This information is vital for understanding the site's hydrological context, which could significantly impact the construction planning and design of the Leon Valley Baptist Church-Recreational Center. The findings of this study will provide essential insights to inform decision-making throughout the project development process.



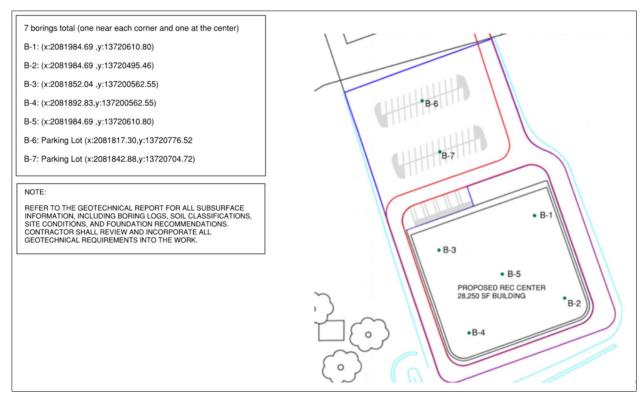


Figure 2: Boring Location Plan

Foundation

The foundation design for the recreation building will be developed directly from these results, which provide key information on soil stratigraphy, strength, and plasticity. By understanding that the upper soils consist of medium-dense clayey sands underlain by very sandy lean clays with moderate to high plasticity, engineers can specify appropriate allowable bearing capacities, embedment depths, and subgrade improvements to ensure a stable, durable system. The test results ensure that the recommended slab on grade with grade beams is appropriately supported. Settlement risk is minimized, and shrink-swell behavior is controlled, resulting in a safe, cost-effective foundation solution tailored to site conditions. Figure 3 illustrates the foundation design layout and foundation design calculations can be found in Appendix D.



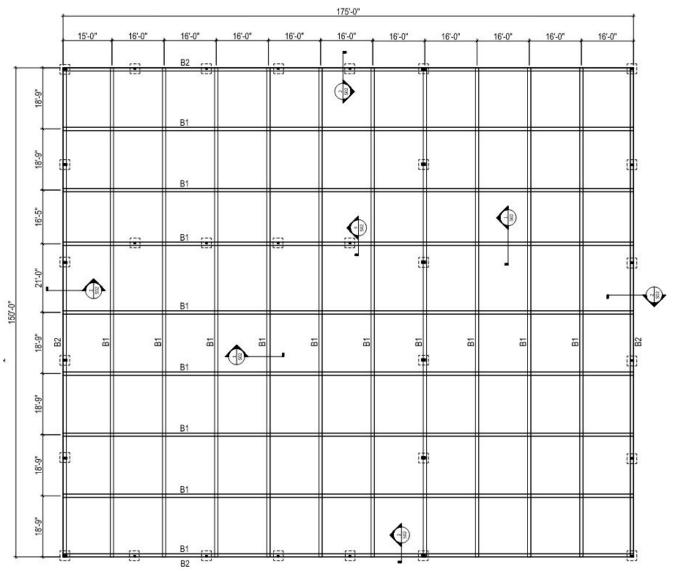


Figure 3: Foundation Design Layout

Water Resources

This report presents the findings of the drainage analysis conducted for the proposed recreation facility. The objective was to evaluate the existing drainage conditions and design a suitable drainage solution to accommodate the proposed recreational facility, asphalt parking lot and perimeter fire access lane.

Existing Drainage

Using USGS Quad Lidar data, an overall existing drainage assessment was performed to analyze the current drainage infrastructure and flow patterns for the existing church property and the additional property to the south.



Analysis determined that the existing church pavement to the north drained east to west directly into the greenway via shallow swales in the pavement. These areas do not affect the new property addition to the south.

The property addition to the south was then split into multiple drainage areas that flow south directly into Culebra Creek greenway. Proposed elements were overlaid to determine which areas were affected by the adverse impacts of adding impervious cover. Existing conditions assessment is shown in Table 1 below. These are the established pre-development discharge flows.

Subbasin ID	Area		Base CN	Impervious Cover %	Тс	Q1	Q ₅	\mathbf{Q}_{25}	Q ₁₀₀
	(AC)	(SQMI)			(MIN)	(CFS)	(CFS)	(CFS)	(CFS)
DA-1	1.4	0.00214	76	-	8.4	0.9	2.7	5.4	8.20
DA-2	1.2	0.00191	76	-	7.7	0.8	2.4	5.0	7.50
DA-3A	4.9	0.00759	76	5	11.9	3.6	9.2	17.9	26.50
DA-3B	3.7	0.00583	76	-	5.8	2.7	8.1	16.5	24.90
TOTAL	11.2					8.0	22.4	44.8	67.10

Table 1: Existing SCS Unit Hydrograph Peak Flow Calculations

Proposed Drainage

To address the needs of the proposed recreational facility, an open ditch system around the site perimeter has been designed, along with a detention pond to intercept additional discharge and mitigate adverse impacts on existing conditions.

Flow from the parking lot, building, and fire lane flows directly into the grass-lined ditches via direct runoff from the pavement. These areas have been split into two drainage areas — West and East — using a crowned section through the center of the proposed addition.

Rational Method for the ditches. For the ditch design, Q = CiA was used, where C is the runoff coefficient, i is the rainfall intensity, and A is the drainage area. The proposed ditch design will be comprised of a V-bottom and 6:1 side-slopes, with a normal depth of 18". The section has been sized using Manning's Equation, combining the hydraulic radius, the flow cross-sectional area, the channel slope, and the roughness coefficient. The ditch material will consist of a grass lining throughout and a rock gabion mattress at the outlet to prevent erosion.



Intensity for each event has been derived from the Intensity-Duration-Frequency (IDF) Values for PA-3, with a time of concentration derived using following " T_c = T_t + T_{sc} + T_{ch} " located in the Storm Water Design Criteria Manual – June 2025.

The peak runoff from the facility has been analyzed for the 1-year, 5-year, 25-year, and 100-year storm intensities, based on the local hydrologic data using the SCS Unit Hydrograph method for the pond the 24 hr duration. Excess runoff from the storm resulted in 1.35 ac-ft of water.

The pond sizing has been calculated and shown below in Table 2 - 4.

Table 2: Proposed SCS Unit Hydrograph Peak Flow Calculations

Subbasin ID	Area		Base CN	Impervious Cover %	Тс	Q1	Q5	Q25	Q100
	(AC)	(SQMI)			(MIN)	(CFS)	(CFS)	(CFS)	(CFS)
DA-1	1.3	0.00195	76	-	8.4	0.8	2.4	4.9	7.50
DA-2	1.2	0.00189	76	-	7.7	0.8	2.4	4.9	7.40
DA-3A	5.0	0.00781	80	55	8.1	13.8	22.7	34.5	45.30
DA-3B	3.7	0.00583	76	-	5.8	2.6	7.8	15.9	24.10
TOTAL	11.2					18.0	35.3	60.2	84.30
DELTA FROM						10.0	12.9	15.4	17.20
EXISTING						10.0	12.9	15.4	17.20

Table 3: Detention Pond Elevation and Storage Values

Elevation (FT)	Incremental Volume (CF)	Cumulative Volume (CF)	Acre Feet	Surface Area (SF)	Acre
797.00	0.77	0.77	0.00	16632.43	0.38
797.50	8576.69	8577.46	0.20	17679.55	0.41
798.00	9104.33	17681.79	0.41	18742.08	0.43
798.50	9639.00	27320.79	0.63	19818.56	0.45
799.00	10180.76	37501.55	0.86	20909.07	0.48
799.50	10729.57	48231.12	1.11	22013.78	0.51
800.00	11285.29	59516.41	1.37	23132.56	0.53
800.50	11848.45	71364.86	1.64	24265.58	0.56
801.00	12418.55	83783.41	1.92	25412.73	0.58



Storm	WSE (FT)	Peak Inflow (CFS)	Peak Discharge (CFS)
5 YR	798.20	22.70	4.70
25 YR	798.70	34.50	8.00
100 YR	799.10	45.30	10.80

A 10-ft gravel maintenance access road to match existing grade has been provided, from the northern side of the property to the detention pond bottom. Regular maintenance of the ditch and detention pond is recommended to prevent sediment build-up and vegetation overgrowth.

Drainage Summary

The property addition will discharge into a detention pond designed to contain the 5-year, 25-year, and 100-year storm events at peak discharge, ensuring no adverse impacts on downstream properties. This aligns with the property's natural drainage patterns and meets local regulatory requirements.

Utilities

This report outlines the planning and design considerations for the utility systems required to serve the proposed Leon Valley Baptist Church Recreation Facility. The objective of the design is to provide reliable domestic water, fire protection, sanitary sewer, irrigation water, and electrical service while maintaining full compliance with the City of San Antonio Unified Development Code (UDC), SAWS Utility Service Regulations, the 2024 International Fire Code as amended by the City of San Antonio, the 2024 International Plumbing Code, and applicable TCEQ standards. The existing church property is currently served by public water, sewer, and electrical utilities along Grissom Road and at the southern edge of the site; however, no direct utility connections exist at the new recreation center's location. Therefore, new utility extensions and laterals will be constructed to support the building.

For water service, a new 2-inch domestic line, a 6-inch fire line, and a 2-inch irrigation branch will extend approximately 670 linear feet from the existing public water main to the facility. The domestic line was sized using the 2024 IPC



Appendix G Water Supply Fixture Unit (WSFU) method. Based on ten water closets, ten lavatories, and eight showers, the total fixture load equates to approximately 152 WSFU, corresponding to a peak demand of roughly 57 gpm per IPC Appendix E, Table E103.3(3). Hazen-Williams calculations confirm that a 2-inch line provides this flow at an acceptable velocity of approximately 5.1 ft/s.

The fire protection system, which includes a full NFPA 13 automatic sprinkler system and one private on-site hydrant, requires a dedicated 6-inch fire service in accordance with NFPA 24 and SAWS fire protection standards. Per the 2024 City of San Antonio Amendments to IFC Appendix G, the base fire-flow requirement for a Type V-B building of approximately 26,250 sq ft is 3,000 gpm for 3 hours (Table B105.1). Section B105.2 allows a 50% reduction for fully sprinklered buildings, resulting in a required design fire flow of **1,500 gpm for 2 hours**. The 6-inch fire line meets NFPA 24 minimum fire main sizing requirements and is routed through a double-check detector assembly (DCDA) as required by SAWS.

Fire department access for the recreation center complies with IFC requirements via the existing drive aisle off Grissom Road, providing the required 150-foot apparatus access distance to all exterior portions of the building. Hydrant coverage is achieved through two existing public hydrants on Grissom Road and the proposed private hydrant located at the southeast corner of the building. Hose-lay distances conform to IFC Section 507.5.1, and final hydrant placement will be coordinated with the Fire Marshal's Office during permit review.

A new 6-inch building lateral discharging will provide sanitary sewer service to a proposed 8-inch private sewer main extension, which will then connect into the existing 42-inch public sewer located on the south side of the site. The lateral incorporates four cleanouts—one at the building and three spaced at 100-foot intervals—in accordance with SAWS Utility Service Regulations and standard wastewater design practice.

Wastewater generation was calculated using TCEQ 30 TAC 285.91(3), Table III, which classifies the facility as a recreation building with showers. Using a building area of 50 square feet per person, the estimated daily occupancy is 525 persons. At a TCEQ loading rate of 15 gallons per person per day, total wastewater generation is 7,875 gallons per day. SAWS applies a standard conversion of 200 gallons per day per Equivalent Dwelling Unit (EDU), resulting in approximately 40 EDUs for impact fee and system capacity evaluation.



Irrigation demand for the facility was assumed to be 60 gpm based on standard commercial rotor zone sizing. Per Irrigation Association design guidelines, typical commercial rotors operate at 0.5–1.0 gpm per head, with approximately 8–12 heads per zone and 4–6 zones operating during peak irrigation scheduling, resulting in a design mainline flow of 50–60 gpm. The proposed 2-inch irrigation branch adequately serves this flow.

CPS Energy will provide electrical service for the building via the existing underground distribution corridor along the southern boundary of the property. Transformer specifications, conduit routing, and metering requirements will be finalized through CPS Energy's design coordination process. They will ensure adequate capacity for HVAC, lighting, and equipment loads with appropriate allowance for future expansion.

All proposed utility alignments have been designed to comply with SAWS, CPS Energy, TCEQ, and City of San Antonio standards. Required horizontal and vertical separations between utilities have been maintained throughout the site, and alignments have been coordinated with architectural, structural, and drainage features. Construction sequencing will prioritize installing underground utilities before paving and structural work to avoid conflicts and maintain long-term serviceability.

Appendix G contains the completed SAWS sewer design sheet, wastewater calculations, and the handwritten domestic, irrigation, and fire service sizing worksheets used to support this design.

Structural

This report summarizes the preliminary structural design of the roof system and columns for a proposed recreation center with total dimensions of 150 feet by 176 feet. The stepped roof and distinct zones within the structure will create separate areas, including a gymnasium equipped with a basketball court and a smaller multi-purpose room marked for volleyball or multiple pickleball courts. The gymnasium area will measure 150 feet by 110 feet, and this design aims to provide a clear interior span free of intermediate supports, suitable for athletic activities and necessary clearances. Additionally, this section of the structure will feature a lower roof clearance of 12 feet.

Moreover, the center will include an entryway, restrooms, meeting space, and a social space measuring 150 feet by 65 feet, sharing one wall with the gym area.



The design for this portion also focuses on maintaining a clear interior span without intermediate supports, allowing for greater construction flexibility, as all interior walls will function as partitions. The framing concept will utilize long-span steel joists (DLH series) supported by joist girders at two perimeter column lines.

This report evaluates the feasibility of spans, joist and girder spacing, tributary load paths, column layouts, and approximate designs for trusses, girders, and columns. The design considerations adhere to several codes, including the San Antonio UDCs, ASCE 7-22, ACI 318-19 for concrete connections to beams, AISC 360 for all steel components, and TMS 402 for the masonry aesthetic features that will be incorporated into the exterior.

Design loads and combinations have been determined in accordance with ASCE 7-22, taking into account the building's classification as Risk Category III due to its use as a public assembly facility. Dead load contributions consist of a uniform 16.3 psf (pounds per square foot) for superimposed dead loads, supplemented by an additional 10 psf for mechanical and electrical allowances to account for suspended lighting, ductwork, and miscellaneous utilities. The steel roof system contributes an additional 6.3 psf, which includes insulation and purlins. Partition loads will vary based on material and location.

Live loads have been selected according to Table 4.3-1 of ASCE 7-22, with 100 psf applied to the gymnasium, corridor, and lobby areas, and a reduced roof live load of 12 psf. Environmental loads were calculated using site-specific parameters. The ground snow load is 10 psf, which results in a flat-roof snow pressure of 6.3 psf and a balanced design load of 14.3 psf, accounting for exposure and thermal coefficients. Seismic effects are minimal, with parameters of Ie = 1.25, Ie SDS = 0.045, and Ie Seismic Design Category A, indicating negligible seismic demand.

Wind loading is governed by a design speed of 114 mph, categorized under exposure category B. Using the parameters Kd = 0.85, Kz = 0.72, Kzt = 1.0, Ke = 0.97, and a gust factor G = 0.85, the velocity pressure qz is calculated as 23.24 psf. The resultant pressures on the gymnasium are approximately +22.8 psf on the windward face, -15.8 psf on the leeward face, and uplift pressures ranging from -25.1 to -43.6 psf. The lower-profile lobby experiences slightly reduced pressures of +19.4 psf on the windward face, -13.5 psf on the leeward face, and uplift values between -21.4 and -37.2 psf.

Tornado resistance has also been considered due to the region's exposure. Using a reference velocity pressure of 27.16 psf and a velocity coefficient KvT = 1.3,



internal, external, and corner pressures are estimated as -31.8, -41.4, and -51.0 psf, respectively, applied over zone widths of 11 feet for the gym and 4.8 feet for the lobby. The governing load combinations, developed per ASCE 7-22 Section 2.3.1, were analyzed for both roof systems. For the gym and lobby roofs, with 1.2D + 1.6S as the controlling factor, the factored roof load is determined to be 42.44 psf.

Structural steel design is based on LRFD (Load and Resistance Factor Design), with $\phi = 0.9$ for flexure and axial members and $\phi = 0.75$ for bolted and welded connections. Material specifications include wide-flange beams of ASTM A992 Grade 50, angles and channel shapes of ASTM A36, plates of A572 Grade 50, and all bolts conforming to ASTM A325, with threads included in the shear plane. All structural members will be checked for strength (including bending, shear, axial, and combined moments where applicable), serviceability (deflection), and stability (buckling, lateral-torsional buckling, and local slenderness).

Gym Roof Joists

- open-web steel joists spanning the full gym width. **64DLH13**, underslung, with a two-way pitched top chord (1:96).
- Loading:
 - Roof live load and roof self-weight are within the listed joist capacity (approx. 500 plf).
 - Factored flexural demand from combined roof loads is less than the joist design capacity.
- Framing and spacing:
 - \circ Joists span 110 ft (gym direction).
 - Cold-formed steel purlins are spaced at 5 ft o.c., running perpendicular to joists.
- Bracing:
 - Top chord is continuously braced by the purlin lines and roof deck.
 - Bottom chord uplift and lateral stability are provided by L1½×1½×1/8 angles used as horizontal bracing at approximately 22 ft spacing, with additional diagonal braces between about 0.4L and 0.6L every four joists.
 - The bracing layout satisfies required chord brace forces from joist buckling and uplift checks.



Lobby Roof Joists

- open-web steel joists over lobby roof area. **36LH09**, underslung, with a one-way pitched top chord (1:96).
- Loading:
 - Roof live load and self-weight are within the joist's tabulated uniform load capacity.
 - Factored moment demand is less than the rated joist bending capacity.
- Framing and spacing:
 - o Joists span approximately **65 ft** across the lobby.
 - o Purlins run perpendicular to joists at **5 ft o.c.** similar to the gym.
- Bracing:
 - o Top chord is braced by purlins and deck.
 - o Bottom chord is braced using L1½×1½×1/8 angles at about 16′-3″ spacing, with additional diagonal bracing between roughly 0.25L and 0.5L every four joists.
 - Bracing forces are within the capacities of the selected angle members and their connections.

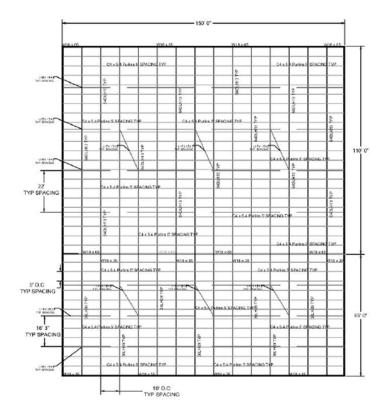


Figure 4: Lobby Roof Joist Diagram



Gym Girders

- W18×65 (A992) spanning 30 ft shall support lines of DLH joists and transfers roof loads to the gym columns.
- Strength and stability:
 - Factored bending moment from truss reactions and self-weight is less than the available flexural capacity, including lateral-torsional buckling effects.
 - Kicker bracing is introduced so that the unbraced length of the compression flange is reduced to 20 ft, which significantly increases the available flexural strength and provides a comfortable margin above demand.
 - Shear capacity of the web is more than the maximum factored reaction.
- Serviceability:
 - Computed girder deflections under service loads satisfy L/360 limits using the provided moment of inertia.

Lobby Girders

- W18×35 (A992) spanning 30 ft shall support LH joists and collect roof loads to lobby columns.
- Strength and stability:
 - Factored bending demand is less than the flexural strength considering lateral-torsional buckling with bracing at 20 ft.
 - Local slenderness of flanges and web is within compact/nonslender limits, and shear capacity comfortably exceeds required shear.
- Serviceability:
 - o Deflection under service load combinations is within L/360, with the provided stiffness (Ix $\approx 800 \text{ in}^4$) exceeding the required inertia.

Exterior Gym Columns (Loadbearing)

- **W14×90** (A992) shall support gym roof girders and resist significant combined axial load and bending from frame action and wind.
- Checks:
 - Strong- and weak-axis slenderness ratios are within acceptable buckling ranges.



- Axial capacity is well above factored axial load (utilization around 20%).
- \circ Combined axial and bending interaction satisfies AISC requirements with a utilization significantly less than 1.0 when using W14×90.
- Shear capacity of the web is adequate for any incidental shear from frame action.

Exterior Lobby Columns (Loadbearing)

- **W6**×**16** (A992) at the lobby perimeter shall support lobby girders and roof framing with primarily axial load.
- Checks:
 - Column slenderness and axial buckling strength have been evaluated; the factored axial load is close to but within the reduced compression capacity.
 - A slightly heavier W6×20 section would be conservative; W6×16 is used with the benefit of framing restraint from adjacent beams and walls.

<u>Interior Gym / Lobby Columns (Shared)</u>

- W12×50 (A992) shall be interior columns supporting both gym and lobby framing where grids align.
- Checks:
 - Axial and slenderness checks show adequate compression strength with a utilization ratio well below 1.0.
 - These columns also provide stiffness for the girder connections and lateral bracing where applicable.

Non-Loadbearing Columns

- Exterior non-loadbearing: W14×38
 - o Supports façade / veneer and acts as a wind frame element, with bending demands within about 90% of available flexural capacity and adequate stiffness for cladding serviceability.
- Interior non-loadbearing: W8×18
 - Supports interior framing and light partitions; bending and shear are well within capacity, and deflection limits are satisfied.



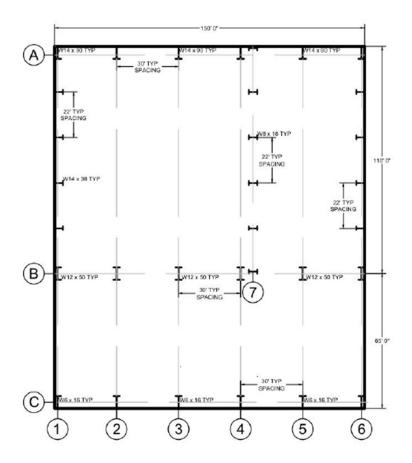


Figure 5: Column Diagram

Truss Bracing

- Gym Trusses:
 - o Top chord braced by roof purlins and deck.
 - Bottom chord bracing uses L1½×1½×1/8 angles arranged as horizontal struts plus periodic diagonals.
 - Member and connection capacities exceed required brace forces derived from truss compression chord demands and uplift.
- Lobby Trusses:
 - Similar bracing scheme with the same angle size but slightly tighter spacing due to shorter span and different brace force demands.

Girder Bracing

- Gym Girders:
 - Lateral-torsional bracing provided by L2½×2½×¼ kicker braces, framing from girder compression flange back to framing points or columns.



 Each brace is designed for the required percentage of girder compression flange force and is checked as a compression member.

• Lobby Girders:

 Braced using L2×2×¼ kicker braces sized for the smaller brace forces of the lobby girders.

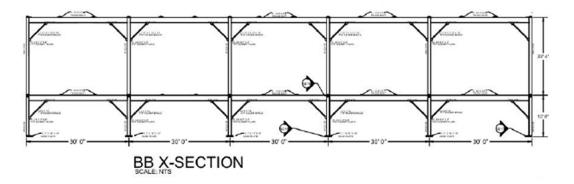


Figure 6: BB Cross Section

Overall, the bracing system provides stability for compression flanges of joists and girders and for column systems, ensuring adequate buckling resistance and controlling lateral displacements.

Roof Purlins

- C4×5.4 cold-formed channels., 5 ft o.c. spanning approximately 10 ft between joists.
- Checks:
 - Flexural demand from roof loads is significantly less than the available moment capacity.
 - Reactions into the joists and connections are small compared to bolt and weld capacities.
 - o Deflections are well within L/360 under service loads.

Wall Girts

- 30 ft bay spacing (typical exterior wall):
 - o Girt type: C8×11.5 spanning 30 ft.
 - o Bending capacity and stiffness are adequate for wind pressures and cladding loads, with utilization well below 1.0.
- Exterior walls with 22 ft spacing:
 - o Girt type: **C6**×**10.5**.



- Designed for wind pressures; flexure and deflection checks are acceptable.
- Interior girts (22 ft span, lower loads):
 - Girt type: C4×5.4, carrying reduced interior loads; strength and serviceability are easily satisfied.

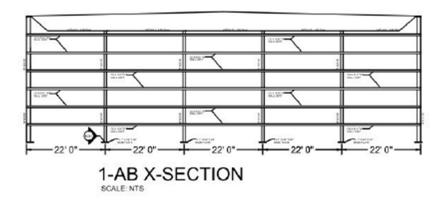


Figure 7: 1-AB Cross Section

Purlin-to-Joist Connections

- L2×2×3/16 clip angle shall with one ½" A325 bolt from angle to purlin and 3/16" fillet welds from angle to joist (both sides, short weld lengths).
- Bolt shear, bearing, and weld strength all exceed the factored reaction from the purlins.

<u>Truss-to-Girder Connections (Gym and Lobby)</u>

- (2) L3×3×¼ angles forming a seat connection where angles are welded to the girder seat plate and to the truss bottom chord.
- Angle axial capacities (yielding and rupture) are several times larger than required truss reactions. Weld sizes (¼" fillet) and lengths are sufficient to develop the angle strength.

Bracing Connections

- Truss bottom-chord brace connection:
 - \circ Small plate welded to truss chord, with 3/16" fillet welds and a single ½" A325 bolt connecting the brace angle.
 - o Both weld and bolt capacities exceed the brace forces.
- Girder brace gussets:
 - \circ 3/8" gusset plates welded to both sides of the girder web.



- o Braces ($L2\frac{1}{2}\times2\frac{1}{2}\times\frac{1}{4}$ for the gym, $L2\times2\times\frac{1}{4}$ for the lobby) are bolted with two bolts each.
- Brace axial capacities and bolt strengths comfortably exceed the required brace forces.

Girder-to-Column Shear Connections

- Gym girders:
 - Shear plate connection using a 3/8" plate with multiple ¾" A325 bolts.
 - Plate bearing, column web bearing, and bolt shear capacities exceed factored reactions.
 - Fillet welds between plate and column are sized to exceed the required shear transfer.
- Lobby girders:
 - Similar shear plate connection at smaller reactions, using a 3/8" plate with two ¾" bolts.
 - Plate and column checks are all satisfactory with ample reserve capacity.

Wall Girt Connections

- Girts are connected to column flanges using two ¾" A325 bolts per connection.
- Bolt capacities exceed the factored girt reactions from wind loading.

Gym Exterior Columns (W14×90)

- Base plate shall be $1\frac{1}{2}$ " $\times 30$ " plate under W14×90.
 - $\circ \hspace{0.1in}$ compression footing with significant overturning.
- Anchors shall be 1¼" diameter anchor rods, arranged with two on the tension side and two on the compression side.
- A ¾" thick stiffener plate welded to the column web improves load transfer to the base plate.
- A continuous 3/8" fillet weld around the column perimeter provides full transfer to the base plate.

Interior Gym / Lobby Columns (W12×50)

• Base plate shall be 1"×20"×20".



- Anchors shall be four **¾" diameter** rods; each rod's tension capacity exceeds factored demands.
- A continuous ¼" fillet weld around the column perimeter provides full transfer to the base plate.

<u>Lobby Exterior Columns (W6×16)</u>

- Base plate shall be ½"×16"×16".
- Anchors shall be 5/8" diameter rods with adequate tension capacity.

Non-Loadbearing Exterior Columns (W14×38)

- Base plate shall be 1"×22"×22" designed for combined moment and small axial load from façade and wind.
- Anchors shall be four **1**½" **diameter** rods providing sufficient tensile resistance.
- 3/8" fillet welds at flanges and web fully develop the column base.

Non-Loadbearing Interior Columns (W8×18)

- Base plate shall be $5/8"\times14"\times14"$.
- Anchors shall be four **7/8" diameter** rods with adequate tension capacity under combined gravity and minor moment.
- Column is fully welded to the base plate with ¼" fillet welds around the perimeter.



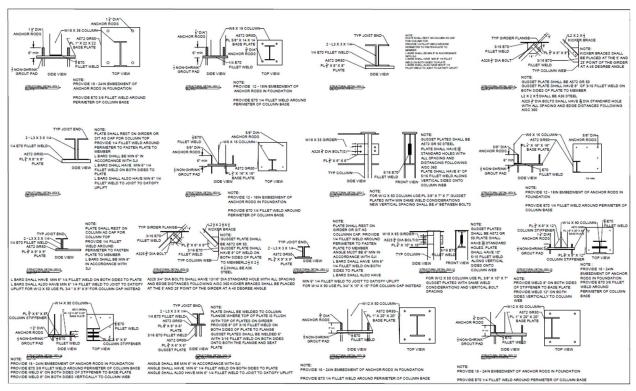


Figure 8: Column/Beam details

Transportation

The Leon Valley Baptist Church campus is located along Grissom Road near Bandera Road in San Antonio, Texas. The existing property includes the main church building and two 24-foot-wide driveways providing access to the site. The proposed Leon Valley Baptist Church Recreational Center will be located behind the existing church and will measure approximately 150 feet by 175 feet (26,250 square feet GFA). The new facility will primarily serve church members and is classified under the City of San Antonio Unified Development Code (UDC) as a Recreational Community Facility (ITE Land Use Code 495).

Grissom Road

Grissom Road runs primarily east-west, with a posted speed limit of 45 miles per hour. The typical configuration of the roadway includes two 12-foot lanes in each direction and a 12-foot Two-Way Turn Lane (TWTL). In 2024, Grissom Road had an Average Annual Daily Traffic (AADT) of 29,493 vehicles.

Trip Generation and Traffic Impact



Based on ITE Trip Generation Manual, 12th Edition (Land Use 495), the proposed 26,250-sf facility is expected to generate approximately 61 weekday PM peakhour trips (29 entering, 32 exiting) under typical weekday programming as illustrated in Table 5. This trip volume remains below the 76-trip threshold that triggers a complete Traffic Impact Analysis (TIA) per City of San Antonio and TxDOT guidelines.

Trip Generation Calculation											
Recreational Community Center - ITE Land Use 495											
1000 Sq. Ft. GFA	· /6 /5 · · · · · · ·				Saturday		Sunday				
Trips/1000 Sq. Ft. GFA		28	.82	1.76		2.31		9.1		13.6	
%Enter/%Exit		50%	50%	66%	34%	47%	53%	50 %	50 %	50 %	50 %
Total Trips		75	57	4	7	6	1	23	39	35	57
Enter/Exit		379	379	31	16	29	32	119	120	179	179

Table 5: Trip Generation Summary (ITE 495)

A TIA worksheet (Appendix J) has been prepared that summarizes projected daily and peak-hour trip generation for normal operations and special event conditions. Under standard use, traffic impacts are minor and can be accommodated within the existing roadway network without requiring intersection or turn lane improvements. However, for special events or large gatherings, estimated peak-hour trip generation may temporarily increase to approximately 65 – 70 trips. These conditions will be mitigated through an Event Traffic Management Plan, including:

- Use of church volunteers to assist with ingress/egress
- Staggered events start and dismissal times
- Temporary on-site signage and traffic control
- Use of overflow parking areas and internal circulation coordination with the existing church lot

Access and Circulation

Vehicular access will remain through the two existing 24-foot-wide driveways along Grissom Road, which currently provide safe and adequate sight distance.



The internal circulation network will connect the existing church parking area to the new recreational center parking lot.

The traffic study will confirm:

- Driveway spacing and alignment with city standards
- Adequate sight distance per TxDOT design criteria
- Compliance with fire lane access (minimum 20 feet clear width)
- Safe pedestrian circulation between the church and the new facility

Turn lane warrants and queueing analyses indicate that no additional turn lanes are required along Grissom Road under existing or projected traffic conditions.

Parking and Bicycle

Parking demand was evaluated in accordance with UDC Table 526-3a for recreational facilities, and the results are illustrated in Table 6.

Table 6: Minimum Code Requirements

Use Classification	Minimum Vehicle Spaces	Maximum Vehicle Spaces		
Recreational Facility (ITE 495)	1.5 per 1,000 sf	10 per 1,000 sf		
Recreational Facility (26,250 sf)	40	262		

Based on the minimum code requirements and anticipated demand for the facility, we have elected to provide parking at a ratio of 2 spaces per 1,000 square feet of gross floor area (GFA), resulting in approximately 52 vehicle spaces. In addition, the site will exceed the minimum accessibility and bicycle standards by including 5 ADA-compliant spaces (with van-accessible design) and five bicycle parking spaces, ensuring adequate accommodation for all users while remaining well within the UDC parking requirements.

Rough Proportionality Analysis

A rough proportionality assessment (Appendix K) was conducted in accordance with the City of San Antonio TIA Guidelines to ensure the proposed improvements are proportionate to the traffic impacts generated by the project. Given that the facility generates fewer than 100 PM peak-hour trips and utilizes existing driveway infrastructure, the required mitigation measures are limited to on-site circulation enhancements, ADA upgrades, and signage improvements. No



off-site roadway or intersection improvements are warranted under current conditions.

Pavement Plan

The Pavement Plan establishes the materials, structural sections, and layout for vehicular pavement areas serving the proposed Leon Valley Baptist Church Recreation Center. The design provides long-term performance under expected traffic loads while meeting City of San Antonio (CoSA) design standards and ADA accessibility requirements.

Pavement Design Criteria

All proposed asphalt pavement materials, thicknesses, and construction practices shall comply with the City of San Antonio Design Criteria Manual (DCM), the Unified Development Code (UDC), and applicable TxDOT Standard Specifications for Construction and Maintenance of Highways, Streets, and Bridges. The pavement section has been designed to support light to medium-duty traffic typically associated with institutional and recreational facilities, including passenger vehicles, church vans, maintenance equipment, and periodic delivery trucks.

Design Parameters

- Design Life: 20 years
- Subgrade Strength: Minimum $CBR \ge 6$, consistent with anticipated native clayey soils in the Leon Valley area
- Traffic Loading: Less than 1,000,000 ESALs, appropriate for non-industrial parking facilities
- Surface Drainage: Positive drainage required toward curb inlets, swales, or approved discharge locations
- Cross Slope:
 - o Asphalt pavement: 1.5%–2.0%
 - o Adjacent concrete surfaces: 2.0% minimum
- Recommended Pavement Structure:
 - o 8 in. compacted granular base (TxDOT Grade 1 or 2, Type B or C)
 - \circ 3 in. hot-mix asphalt (HMA) binder course



 2 in. HMA surface course using Superpave mix with PG 70-22 binder grade (PG 70-20)

Notes and Considerations:

- Pavement thicknesses are based on assumed subgrade conditions; field verification and proof-rolling are recommended prior to construction.
- Superpave surface mix is selected to provide improved rut resistance and performance in high-temperature climates typical of the San Antonio region.
- Base and asphalt lifts must be compacted in accordance with COSA and TxDOT density requirements to achieve structural integrity and long-term durability.
- Additional pavement reinforcement or increased thickness may be required in fire lane areas subject to higher wheel loads.

Traffic Summary and Conclusion

The proposed Leon Valley Baptist Church Recreational Center is expected to integrate seamlessly into the existing church campus, using existing access points and circulation systems. The modest trip generation confirms that a full TIA is not required, and on-site improvements will maintain safe and efficient operation.

By providing compliant parking, ADA access, bicycle facilities, and proactive event management, the project will operate effectively without adversely impacting adjacent roadways or neighboring properties.

Schedule & Budget

The proposed construction schedule for the Leon Valley Baptist Church Recreation Center establishes a structured sequence of work extending from November 2025 through December 2026. The schedule is organized to support the efficient progression of site development, building construction, and commissioning activities while maintaining logical trade coordination.

The project begins with Pre-Construction and Permitting, which allow for regulatory approvals and mobilization activities. This phase is followed by Site Preparation, during which the construction area is cleared, graded, and readied for foundational work. Foundation construction then proceeds as the first significant structural activity.



Subsequent phases include Structural Framing and Roof installation, establishing the primary building structure, and the Building Envelope phase, which provides enclosure and weather protection. With the facility dried in, MEP and utility rough-in is conducted to install essential building systems before interior architectural work.

The schedule then advances into Interior Construction and Finishes, the most comprehensive phase of the project, during which interior walls, finishes, and building systems integration are completed. In parallel, Exterior Site Work addresses paving, drainage, and final grading to ensure site functionality and code compliance.

Following substantial completion of construction activities, the project enters Final Inspections and Commissioning, during which all building systems are tested and validated for operational readiness. The schedule concludes with a Project Closeout phase, encompassing documentation, punch list completion, and turnover to the Owner.

Overall, the planned schedule provides a logical, sequential framework that supports efficient construction, maintains trade coordination, and targets facility completion by late 2026 (406 days) as illustrated in Figure 9.

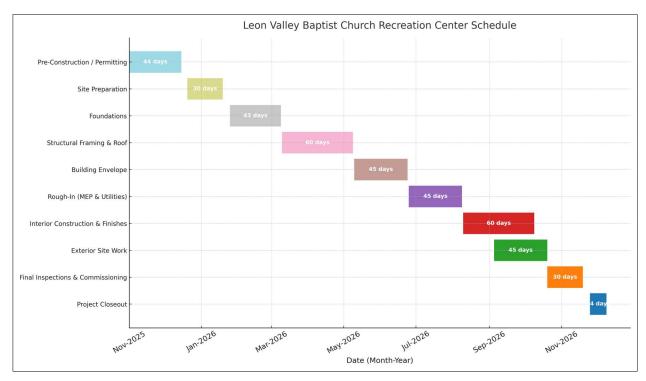


Figure 9: Project Schedule



Cost Summary

A detailed cost estimate was prepared for the proposed Leon Valley Baptist Church Recreation Center to establish an anticipated total project budget and to provide a breakdown of the primary cost drivers as illustrated in Appendix L. The estimate incorporates direct construction costs, building systems, site improvements, engineering and design fees, and associated soft costs. The total projected cost for the facility is \$9,500,000. This estimate provides a comprehensive foundation for project budgeting, funding allocation, and subsequent design-phase refinement.

1. Facility Building Costs — \$4,250,000

These costs represent the core building construction and account for the largest portion of the project budget.

- Main Building Structure \$3,000,000
- Interior Build-Out \$750,000
- MEP Systems \$500,000

2. Construction Materials — \$883,000

Covers materials required to complete the building envelope and interior components.

- Concrete & Rebar \$250,000
- Structural Steel **\$225,000**
- Roofing & Envelope Materials \$200,000
- Finishes & Fixtures \$208,000

3. Site Work — \$550,000

Includes all on-site improvements and utility connections.

- Earthwork & Grading \$200,000
- Paving & Parking \$175,000



- Utilities (Water/Sewer/Electric) \$125,000
- Landscaping \$50,000

4. Structural Components — \$320,000

Structural systems supporting the building.

- Foundations \$140,000
- Slab-on-Grade \$100,000
- Beams/Columns/Girders \$80,000

5. Miscellaneous Construction — \$118,700

Jobsite provisions and temporary work.

- General Conditions \$70,000
- Safety & Temporary Facilities \$48,700

6. Mobilization, Insurance & Bond - \$1,200,000

Contractor startup, insurance coverage, and bonding requirements.

- Mobilization **\$600,000**
- Insurance & Bonding **\$600,000**

7. Construction Contingency - \$1,280,000

Allowance for unknown conditions, design development, and escalation.

8. Engineering & Design Fees — \$888,300

Professional services for planning, design, and engineering coordination.

• Architectural — **\$388,300**



• Civil/Structural/MEP Engineering — \$500,000

9. Permitting, Testing & Administration — \$10,000

Regulatory approvals and quality control.

- Permits \$5,000
- Testing & Inspections \$5,000

Total Project Cost: \$9,500,000



Appendix A – Habitat Compliance





HABITAT COMPLIANCE **FORM**

For information on endangered species habitat within Betar County as may be established, see 2011 Final Recovery Plan for Bexar County Karst Invertebrates, available on US Fish and Wildlife Service's website, https://cocs.bs.gov/doss/recovery_nalmFinal%2009/5308cear*[2006/50]00mretbrates*[20Rech*20Plan_Lpdf] and Management Guidelines for the Golden-checked Warbler in Rural Landscapes by Texas Parks and Wildlife Department available on their website, https://tpwd.texas.gov/publications/pwdpubs/media/psd_bk_w7000_0013_golden_checked_warbler_mgmt.pdf.

Property Owner: Leon Valley Baptist Church	E-mail: Lonestarengineering@lonestar.com
Address: 7980 Grissom Road, San Antonio TX	Zip code: 7980 Phone: 210-755-9000
Agent: Leon Valley Baptist Church	E-mail: Lonestarengineering@lonestar.com
Address:7980 Grissom Road, San Antonio TX	Zip code: 78249 Phone: 210-755-9000
Contact Person Name: Jose Arvizu	E-mail: jose@lonestar.com
Company: Lone Star Engineering	Relationship to Owner: Contracted
Address: 1234 UTSA Boulevard San Antonio TX	Zip code: 1234 Phone: 210-755-9000

Property address or nea	rest street intersection if address	not available:
Acres: 17.434	Ferguson map grid: 15	USGS Grid: Pa-B
In addition to this form	please submit an aerial map de:	signating property boundaries based on the most recently
available imagery. Ma	ps can be obtained from www.sa	nantonio.gov/dsd and saved into a PDF format.

Part 4. Application Type (check one):

☐ Master Development Plan (MDP)	☐ Tree Permit	
Major Plat	☐ Planned Unit Development (PUD) Plan	
☐ Development Plat	☐ Minor Plat	

Part 5. Endangered Species Act Coverage (check one):

Part 3. Endangered Species Act Coverage (check ong):

**The activity subject to the application to the City of San Antonio is covered under an existing individual Section 10(a) permit or an individual Section 7 Biological Opinion analyzing the activity as proposed, and the activity is identical or very similar to the activity proposed in permit and located in the same goographic location. Applicants are supported to the activity proposed in permit and located in the same goographic location. Applicants Section 10(a) permit number (

□ The activity subject to the application to the City of San Antonio is covered by participation in the Southern Edwards Paltacu Habitat Conservation Plan. (SFP HCP) or another approved Regional Habitat Conservation Plan. Applicants checking this box must provide a copy of the Participation Critificate. Complete part 7 of this form, no affidiarity required.

□ The activity subject to the application to the City of San Antonio is not covered by an existing Section 10(a) permit or a Section 7 Biological Opinion no reparticipation in an approved Regional Habitat Conservation Plan. (Complete parts 6, 7 and 8 of this form (if applicable)

Habitat Compliance Form | Updated July 9, 2024 Page 1 of 3



HABITAT COMPLIANCE **FORM**

Part 6. Description for Activities Without Coverage (check one box for both parts A and B):

A. Golden-enceward Warbler Endangered Species		so part or the fract surpect to me appreciation to the City of San Antonio is tocated in the presumptive habitat area for Goldone-theeked Warthers as described below. While this requirement applies throughout the jurisdiction of the City of San Antonio, there is a presumption that areas located outside of Loop 1649, and north of U.S. Highway 99, and west of Interstate Highway 35 do contain habitat. If the property is located in the Leave of the City of San Antonio is the City of San Antonio is the City of San Antonio is children as presumptive habitat areas occurring habitate types to the City of San Antonio is children as presumptive habitat areas occurring habitate types the City of San Antonio is children as presumptive habitat areas occurring habitate types the City of San Antonio is children as presumptive habitat areas occurring habitates the City of San Antonio is children as presumptive habitat areas occurring habitates are considered for the City of San Antonio is children as presumptive habitates are subject to the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children as presumptive habitates are considered from the City of San Antonio is children and present and the City of San Antonio is children and present and the City of San Antonio is children and considered from the City of San Antonio is children and considered from the City of San Antonio is children and considered from the City of San Antonio is children and considered from the City of San Antonio is children and considered from the City of San Antonio is children and considered from th
	3.□	U.S. Fish and Wildlife (USFWS) Ecological Services Field Office, 10711 Burnet Road, Suite 200, Austin, TX 78758 Biologist Name and permit number Date of Survey/Assessment Biologists have notified that their survey/assessment has been utilized □ Yes □ No The tract or portions of the tract subject to the application to the City of San Antonio is within a presumptive habitat area or contains habitat types that may be used by Golden-checked Warblers as set forth in Management Guidelines for the Golden-checked Warblers as Set forth in Management Guidelines for the Golden-checked Warblers as Set forth in Management Guidelines for the Golden-checked Warblers and Wildlife Department, available on their website, and an Endangered Species Survey has NOT been submitted to U.S. Fish and Wildlife. (Selecting this box requires the applicant to complete the Habitat Compliance Affidavit in part 8 of the form.)
B. Karst Invertebrate Endangered Species		No part of the trust subject to the application to the City of San Antonio is located within karst zone 1 or 2 as identified by the USFWS. (Applicant must provide a map demonstrating that the tract is outside of Karst zone 1 or 2). The tract or portions of the tract subject to the application to the City of San Antonio is located within Karst Zone 1 or 2 as identified by the USFWS and a karst feature survey or Endangered Species Survey has been completed by a Biologist permitted by U.S. Fish and Wildlife and copies have been sent or will be sent to: U.S. Fish and Wildlife (USFWS) Ecological Services Field Office, 10711 Burnet Road, Suite 200, Austin, TX 78758
	3.0	Biologist Name and permit number Date of Survey/Assessment Biologist has been notified that their survey/assessment has been utilized \(\to Yes \) No The tract or portions of the tract subject to the application to the City of San Antonio is located within Karst Zone 1 or 2 as identified by the USFWS and a karst feature survey or Endangered Species Survey has NOT been submitted to US. Fish and Wildlife, (Selecting this hor requires the applicant to complete the Habitat Compliance Affidavit

Page 2 of 3 Habitat Compliance Form | Updated July 9, 2024



HABITAT COMPLIANCE **FORM**

Part 7. Owner or Authorized Representative (form is considered incom	plete without thi	s part of the form completed):
I certify that the information provided in	this Habitat Complianc	e Form is true a	and accurate.
Print Name: Jose	Title Engir	neer	
Signature:	Date: 10/30	0/2025	
□ Owner	Authorize	d Representative	
	☐ I affirm the owner.	nat I am authoriz	ed to sign this form on behalf of
Address: UTSA Boulevard	City:San Antonio	State TX	ZipCode 1234
E-mail: jose@lonestarengineering.com			

Part 8. Affidavit of Compliance (required for properties in karst zones 1 or 2 or located in the area identified as potential habitat as set forth in Management Guidelines for the Golden-cheeked Warbler in Rural Landscapes, Texas Parks and Wildlife Department, available on their website when there is no Section 10(a) permit, Section 7 biological opinion, Regional Habitat Conservation Plan, nor endangered species survey submitted to US Fish and Wildlife:

	Affidavit of Compliance	
Before me, the undersigned authority, on this	day personally appeared	("Affiant") who
being first duly sworn, upon his/her oath states	s:	
My name is	and I am the owner of the property tha	t is the subject of this
application to the City of San Antonio.		
A habitat assessment/survey was not	t conducted or I have elected not to provide	e the information.
Please explain below with an addition	onal narrative why no survey has been cond	lucted or why you have
elected to not provide the information	on:	
L as the owner, understand that I am responsi	ible for the property's compliance with the	Endangered Species Act.
Signed this day of		
Signed this day of		
Signed this day of		
Signed this		•
Signed this day of		

Habitat Compliance Form | Updated July 9, 2024



Appendix B – SWPPP Example





TCEQ TPDES CGP
EPA NPDES GCP
Inspection of Controls Report

Complete this form every seven days and retain in your SWP3.

	General Info	rmation	
Name of Project: LEON VALLEY BAPTIST CHURCH - RECREATIONAL CENTER	EPA CGP Tracking No.: TCEQ Authorization No 7779	u:	Inspection Date: 10/30/25
Date of Last Rainfall: 10/28/25	Amount of Last Rainfal	ı: 0.1	
Inspector Name, Title & Con	tact Information	Examp	le, PE, 210-755-9000
Present Phase of Constructio	n	0	
Inspection Location (if multiple specify location where this inspection)		Grissom Ro	ad 78249
site. Check all that apply.) Standard Frequency: Increased Frequency: to	Weekly Every 7 days and within 2 sediment or nutrient-imports, or Tier 3)	4 hours of a 0	n frequencies in different areas of the 0.25° rain (for areas of sites discharging r to waters designated as Tier 2, Tier
Once per month and with seasonally dry periods or Once per month (for froze	in 24 hours of a 0.25" rain during drought) en conditions where earth-	disturbing acti	i-arid, or drought-stricken areas during vities are being conducted)
Was this inspection triggered If yes, how did you detern Rain gauge on site Total rainfall amount that	mined whether a 0.25" s Weather station repre	torm event he sentative of si	as occurred? ite. Specify weather station source:

	CITY OF SAN ANTONIO TRANSPORTATION & CAPITAL IMPROVEMENTS
--	---

CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN FIELD INSPECTION AND MAINTENANCE REPORT

Unsafe Conditions for Inspection
Did you determine that any portion of your site was unsafe for inspection per CGP Part 4.1.5?
Yes No
If "yes", complete the following:
 Describe the conditions that prevented you from conducting the inspection in this location:
Location(s) where conditions were found:
Eccation(s) where conditions were round.

Inspection Type:	Inspected? (Y/N)	Areas of Concern (Describe in detail in the narrative section)
Disturbed Soil Areas	\times	
Material Storage Areas	\boxtimes	
Structural Controls	\times	
Sediment & Erosion Controls		
Entrance(s) and Exit(s)	X	

Discharges:

Nature of discharge (silt, gravel, sand, other pollutant)	Location on-site of discharge		
Lean Clay	North to Center of the property		
Fat Clay	North to Center of the property		
Select fill	North to Center of the property		
Automobile fluid	North		

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CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN FIELD INSPECTION AND MAINTENANCE REPORT

${\bf Best\ Management\ Practices\ Inspected:}\ Add\ additional\ rows\ if\ needed.$

ВМР	Station Number	Left or Right of Center Line	OK (no action required)	BMP failed (describe failure)	Failure due to Maintenance or Improper Design?	Describe corrective actions needed (include schedule)
Detention Pond	01	Left	\boxtimes			
Perm. erosion Control: Sod	02	Left	\boxtimes			
Temp. Erosion Control:Silt Fence	03	Left	\boxtimes			
Temp. Erosion Control:Silt Fence	04	Right	\boxtimes			
Perm. erosion Control: sod	05	Right	\boxtimes			
Sod Irrigation	06	Left	\boxtimes			

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dditional BN	IPs Needed		
Station Number	Left or Right of Center Line	Best Management Practice	Replacing Existing BMP: (Include schedule)

Uni	Uninstalled/Missing BMPs (per SWP3) Station Number Left or Right of Center Line Rest Management Practice Schedule for installing												
Station Number	Left or Right of Center Line	Schedule for installing BMP? (or reason for change)											
l/A													

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SWP3 Updates and Required Recordkeeping Practices

Yes No	Complete all required text fields. Fill out all text fields. Only by filling out all fields will the template be compliant with the requirements of the permit. (Note: Where you do not need the number of rows provided in the template form for your inspection, you may leave those rows blank. Or, if you need more space to document your findings, you may add an additional sheet.)
	Use your site map to document inspection findings. In several places in the template, you are directed to specify the location of certain features of your site, including where stormwater controls are installed and where you will be stabilizing exposed soil. You are also asked to fill in location information for unsafe conditions and the locations of any discharges occurring during your inspections. Where you are asked for location information, EPA encourages you to reference the point on your SWPPP site map that corresponds to the requested location on the inspection form. Using the site map as a tool in this way will help you conduct efficient inspections, will assist you in evaluating problems found, and will ensure proper documentation.
	Sign and certify each inspection report. Each inspection report must be signed and certified by the permittee to be considered complete. Where your inspections are carried out by a contractor or subcontractor, it is recommended that you also have the form signed and certified by the inspector, in addition to the signature and certification required of the permitted operator. The template includes a signature block for both parties.
$\boxtimes \square$	Include the inspection form with your SWPPP. Once your form is complete, make sure to include a copy of the inspection form in your SWPPP in accordance with Part 7.2.12.4 of the CGP.
	and all terms allow accords to the contract of



■ TPDES Certification		
IPDES Certification		
Check One and Complete Signature.		
With the corrective actions noted (if any) and the SWP3.	, the site is in compliance	with the CGP regulatio
The site is in potential non-compliance w non-compliance issues are described below		nd/or the SWP3. Potent
my direction or supervision in accordance w personnel properly gathered and evaluated the the person or persons who manage the sy:	with a system designed be information submitted. stem, or those persons	to assure that qualifi Based on my inquiry directly responsible t
"I certify under penalty of law that this documy direction or supervision in accordance we personnel properly gathered and evaluated the person or persons who manage the sygathering the information, the information is belief, true, accurate, and complete. I am submitting false information, including the pivolations."	with a system designed the information submitted, stem, or those persons submitted is, to the best aware that there are	to assure that qualific Based on my inquiry directly responsible f t of my knowledge as significant penalties f
my direction or supervision in accordance w personnel properly gathered and evaluated th the person or persons who manage the sy- gathering the information, the information s- bellef, true, accurate, and complete. I am submitting false information, including the p	with a system designed the information submitted, stem, or those persons submitted is, to the best aware that there are	to assure that qualific Based on my inquiry directly responsible f t of my knowledge as significant penalties f

Representative's Name (Print clearly): Exampl	Title PE	Date 10/30/25
Representative's Signature:	<u> </u>	<u>'</u>
Example		
Representative's Organization:		
Lone Star Engineering		
Certification Number:		
999021645		

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CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN FIELD INSPECTION AND MAINTENANCE REPORT INPDES Inspection Certification

(Natural gas line projects in Texas are regulated by the EPA)

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing

submitting false information, including the possibility of violations."	fine and in	nprisonment for knowing
Signature of Permittee or "Duly Authorized Representative":	Date:	10/30/25
Printed Name and Affiliation: Example-Lone Star Engineering		
Contractor Notification (City Inspector Use Only)		
Furnish a copy of this inspection report to the Contract inspection. Corrective actions must be taken as soon anticipated rain event, but in no case later than 7 calendar site. If corrective actions are not made within this noncompliance issues, other work on the project may be si	as possib r days after timeframe	le and before the next being able to access the and become potential
Time charges will continue until the project is documentation of corrective action is provided. contractor of liability for noncompliance.		
Contractor's Representative's Name (Print clearly):	Title	Date:
Contractor's Representative's Signature:		
COSA's Representative's Name (Print clearly):	Title	Date:
COSA's Representative's Signature:		'

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Appendix C – Geotechnical Report



	101	*	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377				E	BOF	RINC	3 N	UMI		B -10	
ı	CLIE	NT_	·	PROJEC	T NAME									
ļ	PRO	JECT	NUMBER	PROJEC	TLOCA	TION								_
ı			RTED 8/13/25 COMPLETED 8/13/25					_	HOLE	SIZE	5*		_	_
ı			CONTRACTOR BEA											
ı			Y D. Rocha CHECKED BY R. Burge				LING ING							_
ı			roundwater not encountered during drilling operations.		TER DRI									
Ì					W	N.		z	F.	3	AT	TERBE		FN.
	DEPTH	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT	PLASTIC	PLASTICITY INDEX	FINES CONTENT (%)
			Stratum I - Stiff to very stiff, dark grayish brown FAT CLAY (CH)	SS 1		3-6-7 (13)			16	74	29	45	
			Stratum II - Very stiff to hard, white CHALK		SS 2		10-11-20 (31)							
	5				SS 3		12-21-28 (49)							
42			Stratum III - Hard, tan LEAN CLAY (CL)		SS 4		16-25-33 (58)			10	46	16	30	
NT US.GOT 6/21			- grades tan and light gray in color below 8 feet		SS 5		5-15-19 (34)			13				
CO TOWNWOMESSORY OF	10													
A) 12-29-6376 SHG - CIRC	15				SS 6		4-16-24 (40)							
DEDTECH BHICKLIMMS (BE			Bottom of hole at 15.0 feet.											



		L	Styron Reyes Geotechnical, LLC			E	BOF	RINC	3 N	UMI			
I	S	Ž	16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377								PAG	E 1 0	#- 1
I	CLIE	NT_	<u> </u>	PROJECT NAM	1E								
l			NUMBER	PROJECT LOC									
I	DATE	STAF	RTED 8/13/25 COMPLETED 8/13/25				_	HOLE	SIZE	5*			_
I			CONTRACTOR BEA	GROUND WAT									
I			METHOD Dry Auger			LING							_
I			Y _D, Rocha	AFTER DE		.ING							_
ł			delignated for electrical delignating delignations.	T TENO	1					AT	TERBE	RG	-
I	DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY	FINES CONTENT (%)
l	0				2		ď	ā	-0	_	σ.	5_	E.
			Stratum I - Stiff to very stiff, dark grayish brown FAT CLAY (C	CH) SS		3-6-6 (12)			5	82	33	49	
I													
l				SS 2		7-13-17 (30)			16	86	31	55	
I		7	Stratum II - Hard, light tan CHALK]						
I	5	Ź		SS 3		13-19-27 (46)			9				
I			Stratum III - Hard, tan and light gray FAT CLAY (CH)				1			1			
			- with calcareous deposits from 6 to 8 feet	SS 4		17-19-24 (43)							
		////	- becomes marty below 8 feet		1		1						
200000	10			X 55	:	16-27-33 (60)							
120000000000000000000000000000000000000													
2010 - 2010 4 704 21 11 12	15			SS 6		8-28-35 (63)			12				
00 0 mm 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			Bottom of hole at 15.0 feet.										



ò	*	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232				E	BOF	RINC	3 N	UME		R B-	
70110	-	Telephone: 210.857.9377											
CLIE	_			ECT NAME								_	_
		RTED 8/13/25 COMPLETED 8/13/25	CROU	IND ELEVA	TION			HO! E	9175	6*			_
				IND WATE			_	HOLE	. SIZE	-			_
		METHOD Dry Auger		AT TIME OF									
		Y D. Rocha CHECKED BY R. Burge		AT END OF									
		roundwater not encountered during drilling operations.		AFTER DRIL									
\vdash											TERBE		E
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY 9 (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT	PLASTIC W	PLASTICITY INDEX	FINES CONTENT (%)
-		Stratum I - Stiff to very stiff, dark grayish brown FAT CLAY (C	H)	Man		8-6-8						_	
				X SS 1		(14)			19	97	30	67	
١.	77	Stratum II - Very stiff to hard, white CHALK		SS 2		10-10-12 (22)							
١.	Ż											Ш	
5	Ξ			SS 3		11-14-22 (36)			13	49	23	26	
Ι.		Stratum III - Very stiff to hard, tan LEAN CLAY (CL)		1,			1					\Box	
		- with calcareous deposits from 6 to 10 feet		SS 4		11-22-24 (46)							
١.		- becomes tan and light gray in color below 8 feet											
٠				SS 5		8-13-16 (29)			18				
10													
٠													
		- becomes marly below 12 feet											
				SS 6		17-37- 50/3*			12	49	19	30	
15		Bottom of hole at 15.0 feet.					1					\Box	
		DOMESTI OF TIME OF TOTAL POOL.											



,	*	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377				E	BOF	RING	3 N	UMI		R B-	
CLIE	NT		PPO I	ECT NAME									
	_			ECT LOCA	_								_
DAT	E STA	RTED 8/13/25 COMPLETED 8/13/25	GROU	IND ELEVA	ATION			HOLE	SIZE	5*			
				IND WATE									
DRIL	LING	METHOD Dry Auger		AT TIME OF	DRIL	LING							_
		Y D. Rocha CHECKED BY R. Burge		AT END OF	DRILL	JING							_
NOT	ES <u>G</u>	roundwater not encountered during drilling operations.	-	AFTER DRIL	LING		_	_	_	_			_
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Isf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)		PLASTIC WEBE		FINES CONTENT (%)
-		Stratum I - Hard, dark brown FAT CLAY (CH)		ST 1			4.5+						
		Stratum II - Hard, light tan CHALK		ST 2			4.5+		9	47	21	26	
5				SS 3		13-24-24 (48)			10				
		Stratum III - Very stiff to hard, tan and light gray LEAN CLAY - becomes marly below 8 feet	(CL)	SS 4		8-12-10 (22)							
10				SS 5		9-18-23 (41)			13				
15		Bottom of hole at 15.0 feet.		SS 6		8-21-34 (55)							
		Bostom of hose at 15.0 feet.											



101	¥	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377				E	BOF	RINC	3 N	UMI		R B-	05)F 1
CLIE	NT		PRO IE	CT NAME	,								
	_	NUMBER		CT LOCA									_
DATE	STAF	TED 8/13/25 COMPLETED 8/13/25	GROUN	ND ELEVA	ATION			HOLE	SIZE	5*			
DRIL	LING	CONTRACTOR BEA	GROUN	ND WATE	R LEV	ELS:							
		METHOD Dry Auger	A	T TIME OF	DRIL	LING							_
		Y D. Rocha CHECKED BY R. Burge				ING							_
NOTE	S <u>G</u>	oundwater not encountered during drilling operations.	A	FTER DRIL	LLING								_
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (1st)	DRY UNIT WT. (pdf)	MOISTURE CONTENT (%)		PLASTIC WITE LIMIT		FINES CONTENT (%)
	7	Stratum II - Stiff to hard, light tan CHALK		SS 1		4-5-8 (13)			7	50	24	26	
				SS 2		11-12-18 (30)			3	45	20	25	
5		Stratum III - Hard, tan and light gray LEAN CLAY (CL) to FAT	r CI AV	SS 3		11-21-30 (51)							
		(CH); marly	CONT	SS 4		14-23-26 (49)							
10				SS 5		8-19-21 (40)			11				
15				SS 6		9-17-30 (47)			14	54	20	34	
		Bottom of hole at 15.0 feet.											



101	*	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377				E	BOR	RINC	S NI	UMI		B- 6	
CLIE	NT		PROJEC	T NAME									
PRO.	ECT	NUMBER	PROJEC										
DATE	STAF	TED 8/13/25 COMPLETED 8/13/25	GROUNI	ELEVA	TION			HOLE	SIZE	5*			
DRILL	LING	CONTRACTOR BEA	GROUN	WATE	R LEV	ELS:							
		METHOD Dry Auger				LING							_
		Y D. Rocha CHECKED BY R. Burge				ING							-
NOTE	S <u>G</u>	oundwater not encountered during drilling operations.	AF	TER DRIL	LING		_	_					=
O DEPTH	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)		PLASTIC WITH	PLASTICITY 2	FINES CONTENT (%)
		POSSIBLE FILL - Brown sandy day		SS 1		12-15-16 (31)							
		Stratum III - Hard, tan and light gray LEAN CLAY (CL)		SS 2		16-19-22 (41)			9	48	21	27	
5		- marly from 4 to 8 feet		SS 3		11-21-28 (49)							
		- grades to hard, tan and light gray FAT CLAY (CH) below 8 f	lood	SS 4		16-25-29 (54)			11	46	17	29	
10		- glades to hard, can and light glay PAT CLAT (CA) below of	001	SS 5		14-26-30 (56)			13				
				<i>M</i>									
15		Bottom of hole at 15.0 feet.		SS 6		7-19-26 (45)			14				98
		DOMENT OF TIONE OR 15.0 FEBT.											



101	*	Styron Reyes Geotechnical, LLC 16100 Henderson Pass #160 San Antonio, Texas 78232 Telephone: 210.857.9377				E	BOF	RINC	3 N	UMI		R B-	
CLIE	NT		ROJEC	T NAME									
				TLOCA									
DATE	STAF	RTED 8/13/25 COMPLETED 8/13/25 G	ROUN	ELEVA	ATION		_	HOLE	SIZE	5*			
DRIL	LING			WATE									
DRIL	LING	METHOD Dry Auger	AT	TIME OF	DRIL	LING							
LOGG	GED B	Y D. Rocha CHECKED BY R. Burge	AT	END OF	DRILL	ING							
NOTE	S <u>G</u>	roundwater not encountered during drilling operations.	AF	TER DRI	LLING								
				Ψ	26		-j	ı.	3		ERBE		F.
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY (RQD)	BLOW COUNTS (N VALUE)	POCKET PER (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%	LIMIT	PLASTIC	PLASTICITY	FINES CONTENT (%)
0	8888	FILL - Brown clayey sand	_		-		-	-			-	u.	-
				SS 1		4-6-12 (18)			11	55	24	31	
-													
-				SS 2		12-19-23 (42)							
├ -	~~	Stratum II - Hard, tan CHALK		_			1						
	7			1									
- 5	7			X SS		15-32- 50/4"			8				
	7			/\					_				
1	/////////////////////////////////////	Stratum III - Hard, tan and light gray LEAN CLAY (CL)											
		- marly below 6 feet		SS 4		24-32-39 (71)							
				SS 5		12-17-27 (44)			11				98
10													
		- grades to very stiff, tan and light gray FAT CLAY (CH) below 12	2 feet										
15				SS 6		6-9-19 (28)			12	60	18	42	
		Bottom of hole at 15.0 feet.											



Appendix D – Foundation Slab-on-Grade Design Calculations



Geotechnical Exploration Plan (8 Borings)

Building footprint: $150 \text{ ft} \times 175 \text{ ft}$

Foundation concept (anticipated): Shallow spread footings + slab-on-grade (recreational floor use)

Number of borings: 5 (four corners inset + one center) 3 in parking lot

Exploration depth target: 15 ft below existing grade (extend if soft/organics/loose sands or until

competent stratum/refusal)

Even though $roof+dead \approx 35 \text{ psf}$ is light, column/footing reactions can still influence 2 – 3B below footings (B = footing width). A 3 – 4 ft footing implies 6 – 10 ft influence depth; exploring to 15ft ensures we catch deeper soft layers, collapsible sands, or high-PI clays that could drive settlement or slab movement.

Slab-on-Grade

Codes and Design Guides Utilized:

- ASCE 7-16
- IBC 2018
- ACI 318-19
- AISC 360-16,15th Edition
- AISC Design Guide 1
- WRI TF 700-R-07

Stiffened Slab-on-Grade Design

A slab-on-grade foundation for a recreational building consists of a reinforced concrete slab placed directly on prepared and compacted subgrade to provide a durable, uniform, and economical base for the structure. This type of foundation is ideal for large, single-story facilities such as gyms, community centers, or multipurpose halls, where loads are primarily vertical and evenly distributed. The slab typically includes thickened edge and interior grade beams to resist differential settlement and support structural and architectural loads such as walls and columns. Reinforcement is placed within the slab to control cracking due to shrinkage, temperature changes, and minor ground movement. Beneath the slab, a compacted granular subbase and vapor retarder are provided to



enhance stability and protect against moisture intrusion. Designed in accordance with ACI 360R and geotechnical recommendations, the slab-on-grade system offers a low-maintenance foundation capable of supporting both dynamic and static loads common in recreational facilities while ensuring long-term performance and serviceability.

Slab-on-Grade Design Calculations

Effective P.I.= 31

Equivalent PI must be corrected for Slope and Degree of Consolidation.

Effective $PI = Equivalent PI \times Cs \times Co$

Cs = *slope correction coefficient*

Co = consolidation correction coefficient

Using values estimated from Fig. 8 and Fig. 9

(WRI TF 700 R 07):

Equivalent PI = 28

Ground slope = $2.5\% \rightarrow Cs = 1.02$

Unconfined compressive strength \approx 3 TSF \rightarrow Co = 1.10

Effective PI = $28 \times 1.02 \times 1.10 = 31.4 \approx 31$

Site Specifications:

- Effective P.I.= 31
- Climatic Rating, Cw= 17
- Slope = 2.5%
- Unconfined compression, qu = 2,500

Depth (ft)	Soil Stratum	Soil Type	PI	Factor	Factor × PI
0-5	Stratum I	Fat Clay (CH)	46	3	138
5–10	Stratum II	Chalk (NP)	0	2	0
10–15	Stratum III	Lean Clay (CL)	30	1	30
	ΣF = 6				Σ(F×PI) = 168

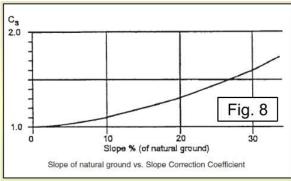
Weighted PI = Σ (F×PI) / Σ F = 168 / 6 = 28

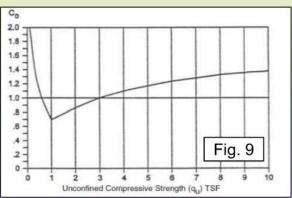
Interpretation

Weighted Plasticity Index = 28 → Moderately Expansive Soil.

Design Implication: For PI = 25–35, classify as Moderate Plasticity.

Recommend stiffened slab-on-grade foundation with uniform moisture control and positive drainage (≥2% for first 10 ft).







Building Specifications:

Building Length = 176 ft

Building Depth = 150 ft

Height = Lobby 12 ft

Gym 35 ft

Slab Thickness = 5in

Loads:

Loads Calculated using ASCE 7-22 as per San Antonio UDC

Dead Load = 16.3psf

Live Roof Load = 12psf

Snow/Rain Load =14.3psf

Wind load = -25.1(gym), -21.4 (lobby)

Load combination(s):

1.4D, 1.2D+1.6Lr+0.5S, 1.2D+1.6S+0.5W

1.2D + 1.6S = 44.24psf (control)

WRI Design Based on Building and Site Specifications:

Slab = rectangle

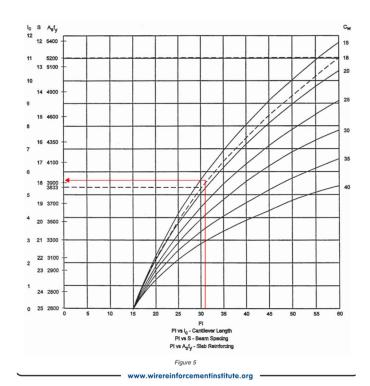
S = 18 ft, max

1c = 5.5

Asfy = 4000

$$K_1 \& K_s = 1$$

Number of Beams in each direction:





Long Beams N = 150/18 + 1 = 9

$$\underline{L}'$$
 Where: S = Spacing ft (m) from Fig. 5
N = S +1 L' = width of slab, ft (m)

Spacing =
$$150/(9-1) = 18' -9"$$

9 beams will be used W-E 18' -9" OC

Short Beams N = 176/18 + 1 = 10 Short Beams

Spacing =
$$176/(10-1) = 19' -6 \frac{3}{4}$$
"

11 beams will be used S-N @16' -0" OC

B individual = assumed 12"

Moment:

Slab load only = 150 pcf x (5-12) ft = 62.5 psf

• Long direction (use L=176 ft):

$$M_L = rac{62.5 imes 176 imes (5.5)^2}{2000} = extbf{166.4} \ ext{kip}^{ackslash}$$

• Short direction (use L=150 ft):

$$M_s = rac{62.5 imes 150 imes (5.5)^2}{2000} = extbf{141.8 kip} ackslash$$

Beam Design:

Beam depths:

$$d_L = \Big(rac{664\,M_L\,\ell_c}{7\cdot 12}\Big)^{1/3}, \qquad d_s = \Big(rac{664\,M_s\,\ell_c}{6\cdot 12}\Big)^{1/3}$$

•
$$d_L=\left(rac{664 imes166.4 imes5.5}{84}
ight)^{1/3}={f 19.34}\ {
m in}$$
 $ightarrow$ say 20–22 in • $d_s=\left(rac{664 imes141.8 imes5.5}{72}
ight)^{1/3}={f 19.30}\ {
m in}$ $ightarrow$ say 20–22 in

•
$$d_s = \left(rac{664 imes141.8 imes5.5}{72}
ight)^{1/3} = {f 19.30} ext{ in}
ightarrow$$
 say 20–22 in

- ullet Moments: $M_L=166.4$ kip·ft, $M_S=141.8$ kip·ft
- $f_c'=3$ ksi, $f_y=60$ ksi, $\phi_{
 m flex}=0.90$
- Cover = 3 in, stirrup = #3 (pprox0.375 in), #6 bar $A_b=0.44~{
 m in}^2$, $d_b=0.75$ in
- Effective depth with h = 24 in:

$$d pprox 24 - 3 - 0.75/2 = \mathbf{20.625} \ ext{in}$$



Required steel:

Using
$$\phi M_n \geq M_u$$
 with $a = rac{A_s f_y}{0.85 f_c' b}$ and $M_n = A_s f_y ig(d - rac{a}{2} ig)$:

- Long (L) dir $\rightarrow A_{s,\mathrm{req}} = 1.98~\mathrm{in^2}$ (was 2.34 in² at h=22)
 - $_{
 m a}=3.88$ in; $\phi M_npprox 1996.8/12=$ 166.4 kip·ft (meets exactly at the solve point)
- Short (S) dir \rightarrow $A_{s,\mathrm{req}} = 1.66 \mathrm{~in^2}$ (was 1.87 in² at h=22)

$$_{
m a}=3.25$$
 in; $\phi M_npprox 1701.6/12=$ 141.8 kip·ft (meets exactly)

#6 Bars w/b=12in we can fit 3 #6 per layer max (≥ 1 " clear).

- Long (need ≥ 1.98 in²)
 - 5-#6 (3 + 2) ightarrow $A_s=2.20~{
 m in}^2$ ightarrow ϕM_npprox 182.8 kip-ft ightarrow 166.4 \checkmark
 - 6-#6 (3 + 3) \rightarrow $A_s=2.64$ in² \rightarrow $\phi M_npprox 214.3$ kip·ft (more reserve)

Exterior beams measure 12 in \times 24 in

Reinforced with 5-#5 bars (2 top + 3 bottom) continuous.

At column lines, add two additional #5 top bars. Shear reinforcement consists of #3 ties at 24 in oc.

Clear spacing: ≥ 1 in (or bar dia); $\geq \sim 1.5$ in vertical clear between layers

- Short (need \geq 1.66 in²)
 - 4-#6 (2 + 2 or 3 + 1) \rightarrow $A_s=1.76~{
 m in}^2$ \rightarrow ϕM_npprox 149.7 kip·ft \geq 141.8 \checkmark
 - 5-#6 ightarrow $A_s=2.20$ in² ightarrow $\phi M_npprox182.8$ kip·ft (extra reserve)

Interior beams range from 12 in \times 24 in.

Each beam includes 4-#5 bars (2 bottom + 2 top) continuous, with two additional

#5 top bars at column intersections. Shear reinforcement uses #3 ties at 24 in oc.

Clear spacing: ≥ 1 in (or bar dia); $\geq \sim 1.5$ in vertical clear between layers

• Lap grade beam and slab reinforcement splices 40 bar diameters (not less than 18in)



 Refer to structural documents for foundation plan, grade beam schedule, typical beam sections, and further slab information.

Slab-on-Grade Design

Assume slab thickness t = 5 in; joints at 12 - 15 ft. Service floor load L = 35 psf (no forklifts).

Self-weight of slab:

$$t = 5 \text{ in} = 5/12 \text{ ft} = 0.4167 \text{ ft}$$

$$\gamma$$
 c = 150 pcf

w slab =
$$\gamma$$
 c \times t = 150 \times 0.4167 = 62.5 psf

q service =
$$w slab + L = 62.5 + 35 = 97.5 psf$$

Bearing check vs allowable contact:

q service =
$$97.5 \text{ psf} \ll \text{qa} = 2,500 \text{ psf} \rightarrow \text{OK}$$

Crack-control reinforcement selection (WRI, PI=23, Cw=17):

Target As $\approx 0.20 \text{ in}^2/\text{ft}$ each way \rightarrow Provide #4 @ 12 in OC EW (As,prov = 0.20 in $^2/\text{ft}$).

Joints: Saw-cut control @ 12 - 15 ft; Isolation joints at columns/grade beams and exterior interfaces.

Two way (punching) shear check (approx.):

Critical perimeter b0 at d/2 from column face: a = 12 in; $d \approx 16$ in

$$b0 = 4 \times (a + d) = 4 \times (12 + 16) = 112 \text{ in}$$

Vu (conserv.)
$$\approx P = 50,000 \text{ lb}$$

$$vu = Vu / (b0 \cdot d) = 50,000 / (112 \times 16) = 27.9 \text{ psi}$$

$$\phi$$
 vc (ACI) $\approx 0.75 \times 2 \sqrt{fc} = 0.75 \times 2 \times \sqrt{4000} = 0.75 \times 2 \times 63.25 = 94.9 \text{ psi}$

$$vu = 27.9 \text{ psi} < 94.9 \text{ psi} \rightarrow O$$



Base Plate & Anchor Bolt Design (Axial, concentric)

Axial bearing only (no net moment). Concrete support at f'c = 4,000 psi, grout bed provided.

Required bearing area (AISC/AISC DG1 approach):

$$\phi$$
 · 0.85 fc · Aplate \geq P (take ϕ \approx 0.65 - 0.75; for a quick check use 0.85 fc

without ϕ for service)

$$0.85 \, \mathrm{fc} = 0.85 \times 4000 = 3400 \, \mathrm{psi}$$

Areq = P /
$$(0.85 \text{ fc}) = 50,000 / 3,400 = 14.7 \text{ in}^2$$

Select base plate:
$$12 \text{ in} \times 12 \text{ in} \times 1 \text{ in} \rightarrow A = 144 \text{ in}^2 >> 14.7 \text{ in}^2 \text{ (OK)}$$

Anchor bolts (uplift/shear not governing for axial only):

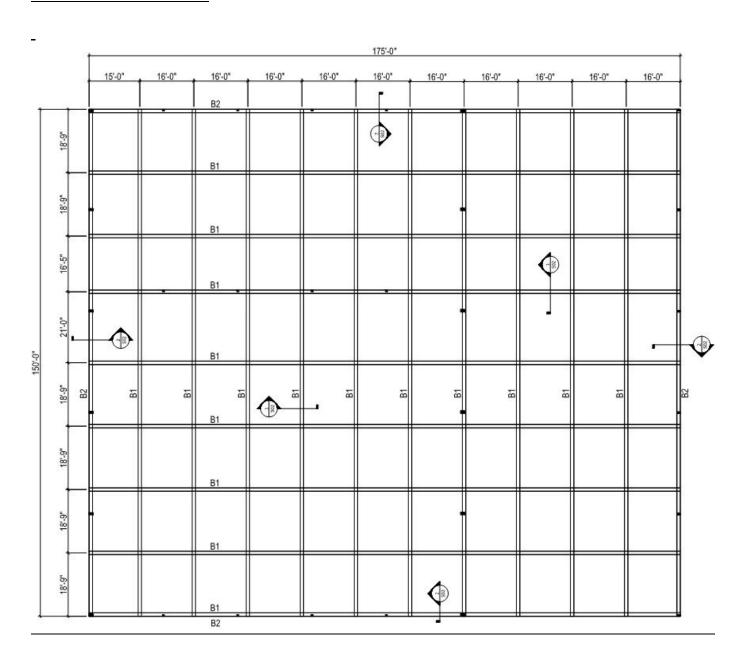
Provide 4- \emptyset 3/4 in F1554 Gr. 55 with 12 in embedment (template with 9 in \times 9 in

bolt circle).

Non shrink grout under plate; 1/2 in grout thickness; leveling nuts/washers; edge distance ≥ 1.5 in

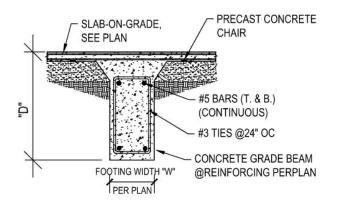


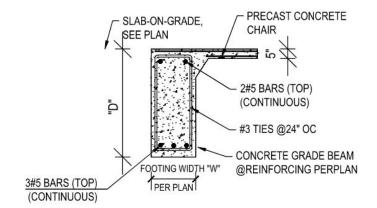
Foundation Floor Plan:





Typical Details:





TYP. INTERIOR BEAM DETAIL

TYP. EXTERIOR BEAM DETAIL



Appendix E – HEC-HMS Results

Project: Sdii

Simulation Run: 100yr_prop

Simulation Start: 7 November 2025, 24:00 Simulation End: 8 November 2025, 06:00

HMS Version: 4.12

Executed: 17 November 2025, 00:14

Global Parameter Summary - Subbasin

Area (MI2)

Element Name	Area (MI2)
DA - 3A	0.01
DA - 3B	0.01
DA - I	O
DA - 2	0

Downstream

Element Name	Downstream
DA - 3A	Reservoir - I
DA - 3B	Creek
DA - I	Creeki
DA - 2	Creek2

Loss Rate: Scs

Element Name	Percent Impervious Area	Curve Number
DA - 3A	55	80
DA - 3B	0	76
DA - I	0	76
DA - 2	0	76

Transform: Scs

Element Name	Lag	Unitgraph Type
DA - 3A	5	Standard
DA - 3B	4	Standard
DA - I	5	Standard
DA - 2	4.6	Standard

Global Parameter Summary - Reach

Downstream

Element Name	Downstream
Reach - I	Creek

Route: Lag

Element Name	Method	Initial Variable	Lag
Reach - I	Lag	Combined Inflow	1.24

Global Results Summary

Hydrologic Element	Drainage Area (MI2)	Peak Discharge (CFS)	Time of Peak	Volume (IN)
DA - 3A	0.01	45.3I	08Nov2025, 00:36	3.34
Reservoir - 1	0.01	10.77	08Nov2025, 00:57	3.09
Junction - 1	10.0	10.77	08Nov2025, 00:57	3.09
Reach - 1	10.0	10.77	08Nov2025, 00:58	3.09
DA - 3B	0.01	24.06	08Nov2025, 00:36	1.92
Creek	10.0	28.31	08Nov2025, 00:37	2.58
DA - 1	O	7.48	08Nov2025, 00:37	1.92
Creekı	O	7.48	08Nov2025, 00:37	1.92
DA - 2	O	7.43	08Nov2025, 00:37	1.92
Creek2	O	7.43	08Nov2025, 00:37	1.92

Subbasin: DA-3A

Area (MI2): 0.01

Downstream : Reservoir - 1

Loss Rate: Scs

Percent Impervious Area	55
Curve Number	80

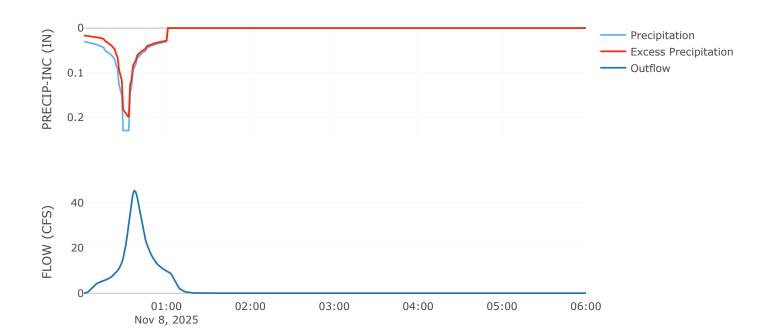
Transform: Scs

Lag	5
Unitgraph Type	Standard

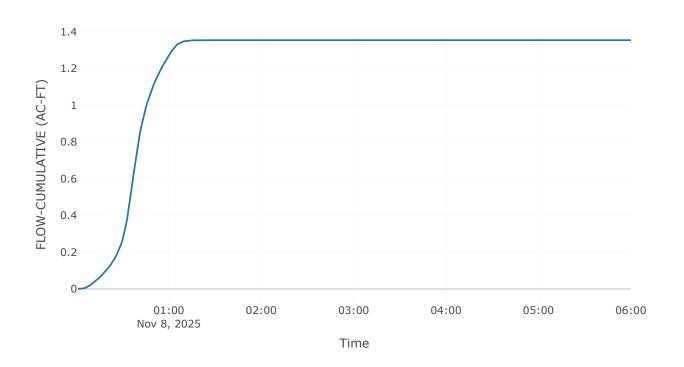
Results: DA-3A

Peak Discharge (CFS)	45.3I
Time of Peak Discharge	08Nov2025, 00:36
Volume (IN)	3.34
Precipitation Volume (AC - FT)	1.72
Loss Volume (AC - FT)	0.36
Excess Volume (AC - FT)	1.35
Direct Runoff Volume (AC - FT)	1.35
Baseflow Volume (AC - FT)	O

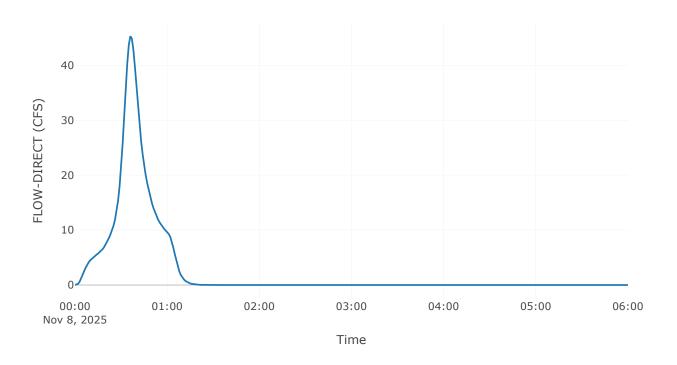
Precipitation and Outflow



Cumulative Outflow



Direct Runoff



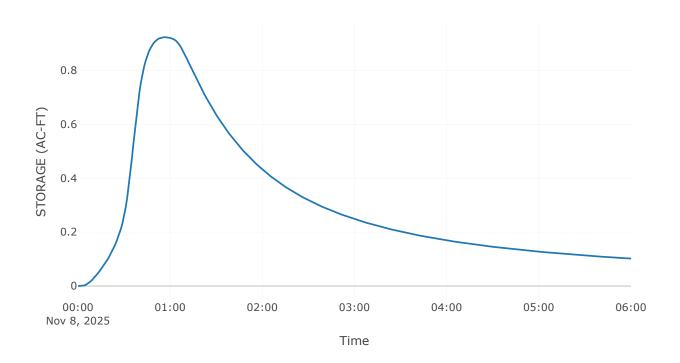
Reservoir: Reservoir-1

Downstream: Junction - I

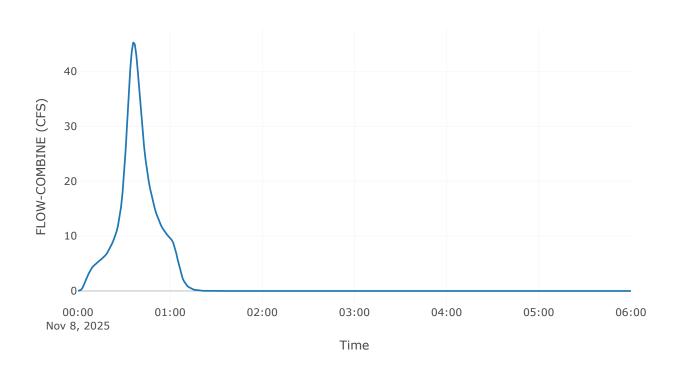
Results: Reservoir-1

Peak Discharge (CFS)	10.77
Time of Peak Discharge	08Nov2025, 00:57
Volume (IN)	3.09
Peak Inflow (CFS)	45.3I
Time of Peak Inflow	08Nov2025, 00:36
Inflow Volume (AC - FT)	1.35
Maximum Storage (AC - FT)	0.92
Peak Elevation (FT)	799.13
Discharge Volume (AC - FT)	1.25

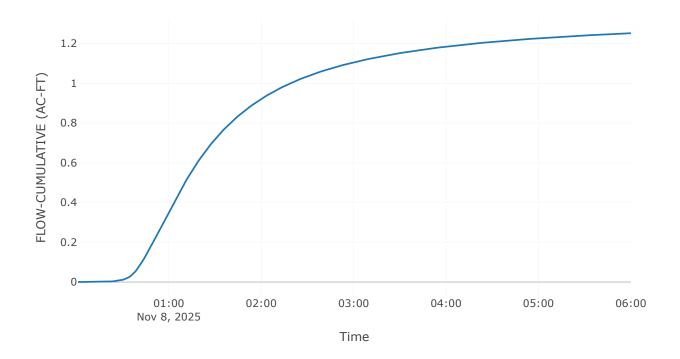
Storage



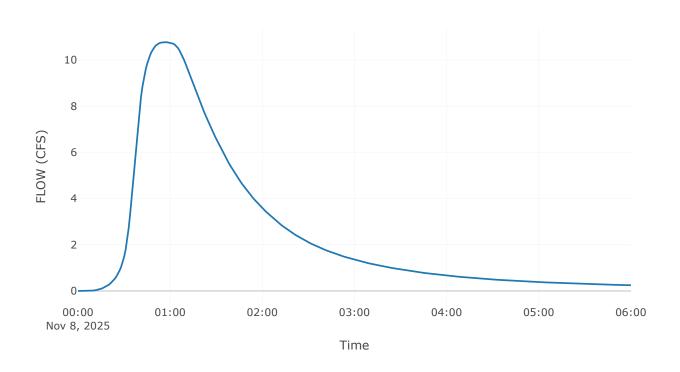
Combined Inflow



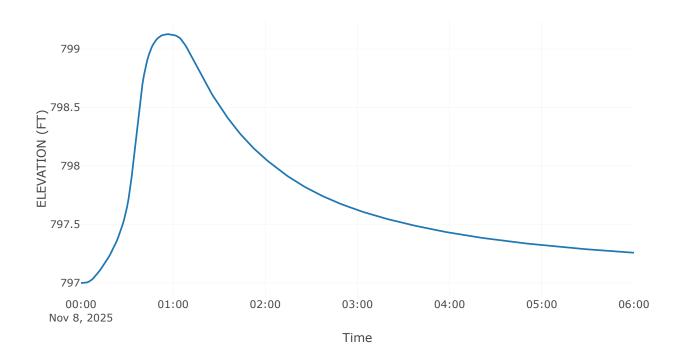
Cumulative Outflow



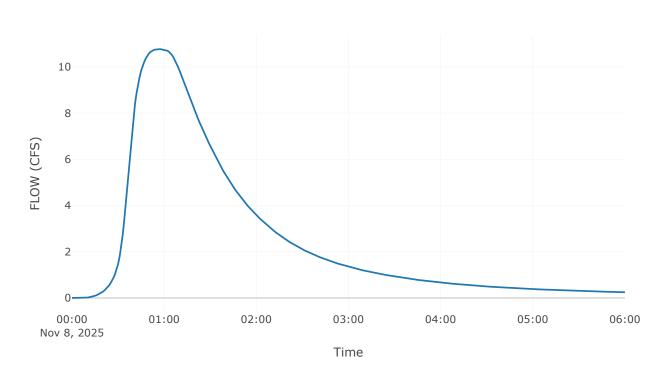
Outlet 1



Pool Elevation



Outflow



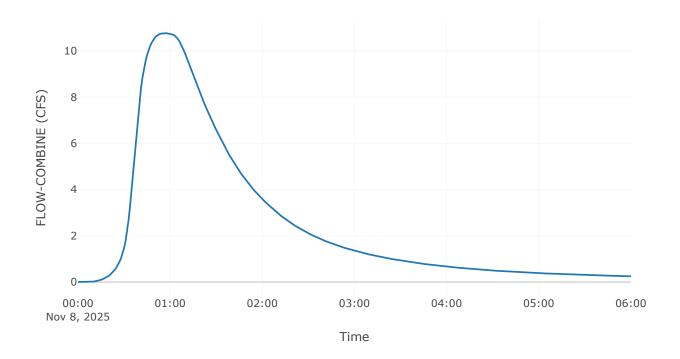
Junction: Junction-1

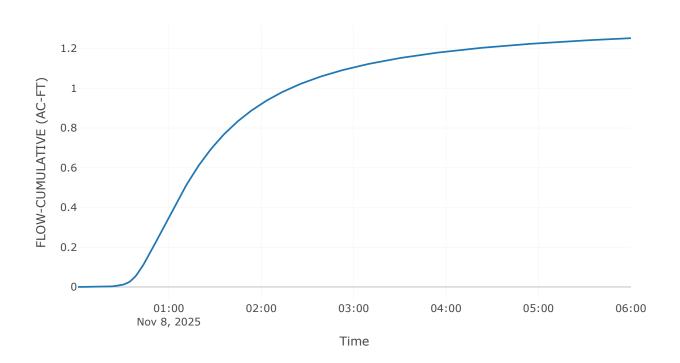
Downstream : Reach - I

Results: Junction-1

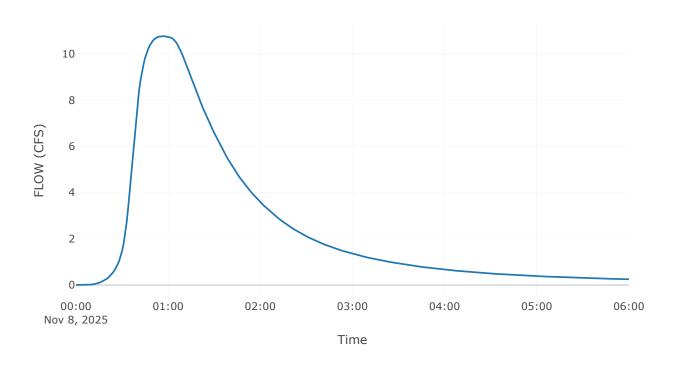
Peak Discharge (CFS)	10.77
Time of Peak Discharge	08Nov2025, 00:57
Volume (IN)	3.09

Combined Inflow





Outflow



Reach: Reach-1

Downstream : Creek

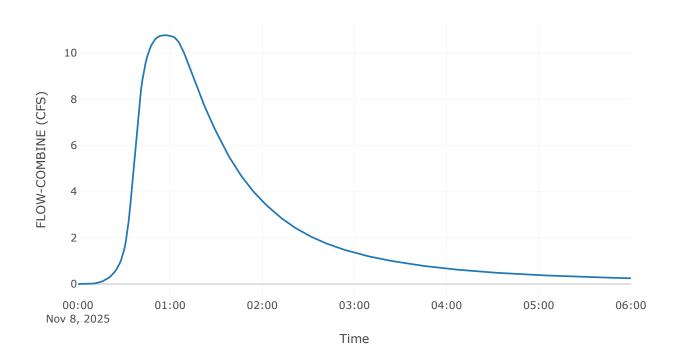
Route: Lag

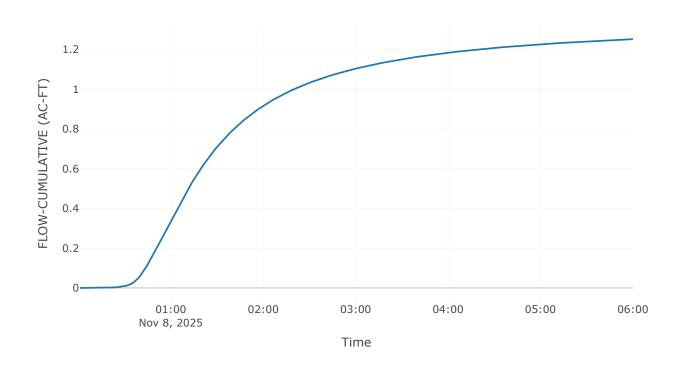
Method	Lag
Initial Variable	Combined Inflow
Lag	I.24

Results: Reach-1

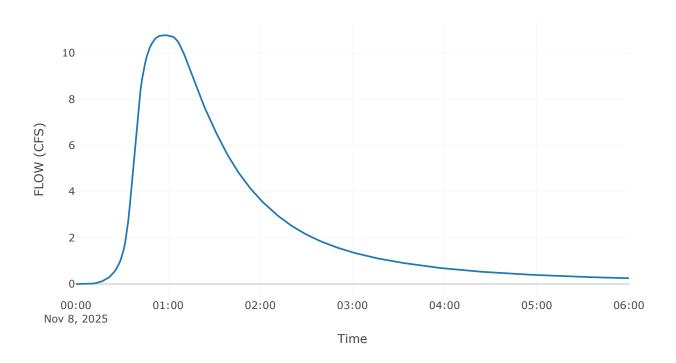
Peak Discharge (CFS)	10.77
Time of Peak Discharge	08Nov2025, 00:58
Volume (IN)	3.09
Peak Inflow (CFS)	10.77
Inflow Volume (AC - FT)	1.25

Combined Inflow





Outflow



Subbasin: DA-3B

Area (MI2): 0.01

Downstream: Creek

Loss Rate: Scs

Percent Impervious Area	0
Curve Number	76

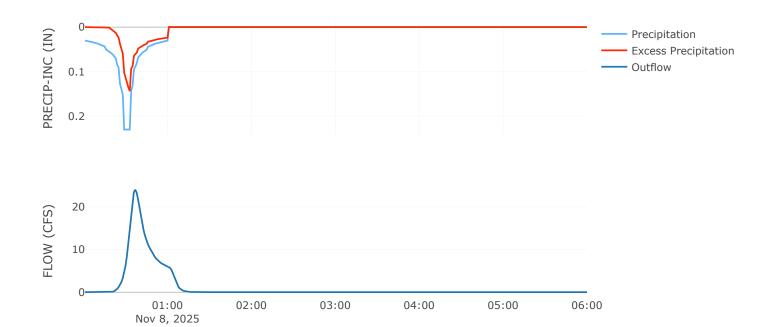
Transform: Scs

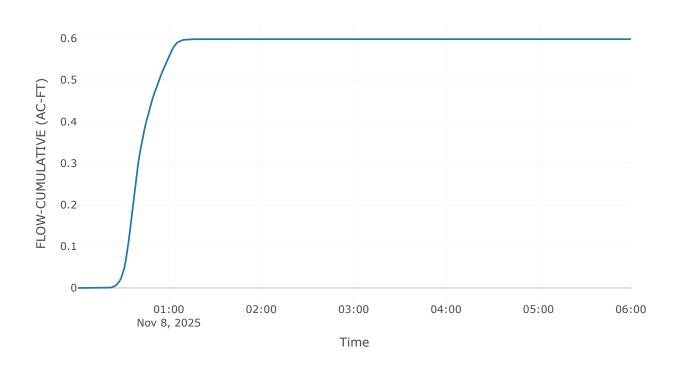
Lag	4
Unitgraph Type	Standard

Results: DA-3B

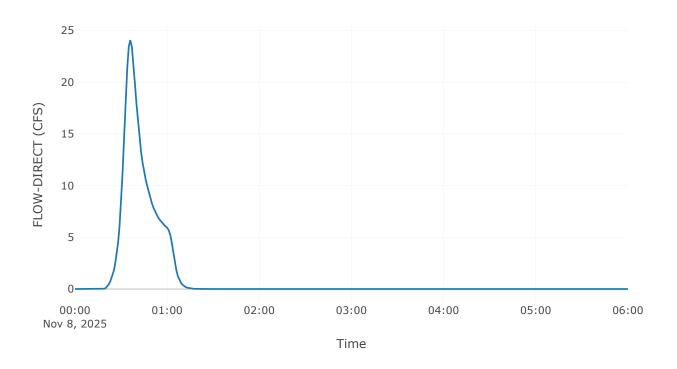
	Results. Dr. 3D
Peak Discharge (CFS)	24.06
Time of Peak Discharge	08Nov2025, 00:36
Volume (IN)	1.92
Precipitation Volume (AC - FT)	1.32
Loss Volume (AC - FT)	0.72
Excess Volume (AC - FT)	0.6
Direct Runoff Volume (AC - FT)	0.6
Baseflow Volume (AC - FT)	O

Precipitation and Outflow





Direct Runoff

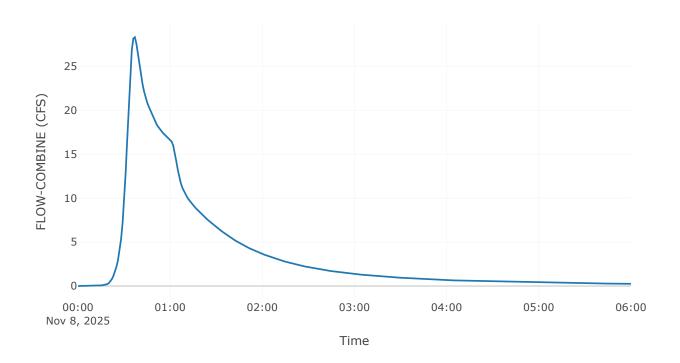


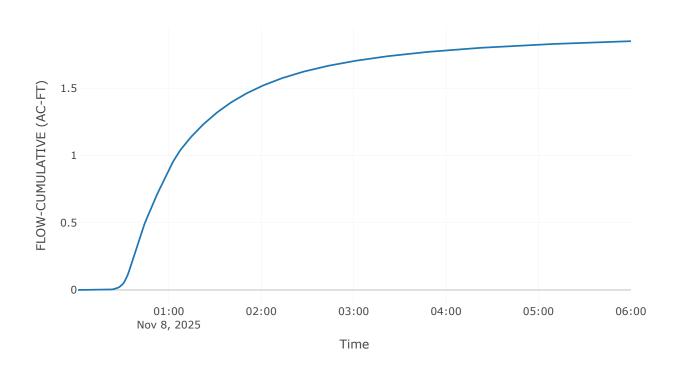
Junction: Creek

Results: Creek

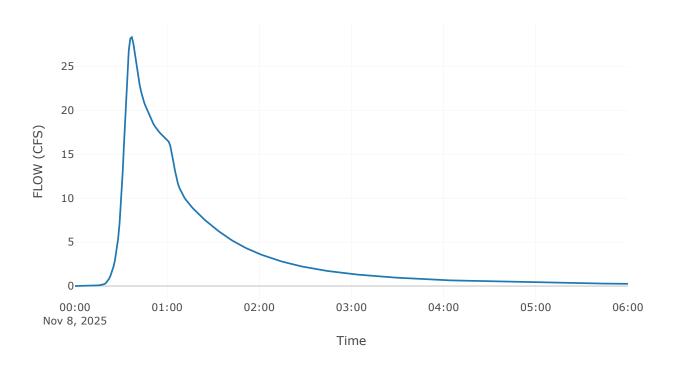
Peak Discharge (CFS)	28.31
Time of Peak Discharge	08Nov2025, 00:37
Volume (IN)	2.58

Combined Inflow





Outflow



Subbasin: DA-1

Area (MI2):0

Downstream : Creekı

Loss Rate: Scs

Percent Impervious Area	O
Curve Number	76

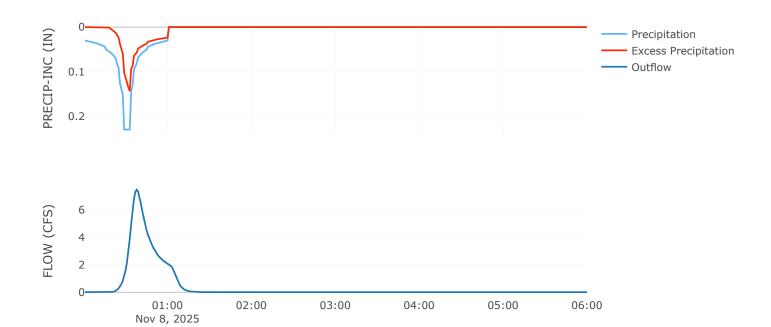
Transform: Scs

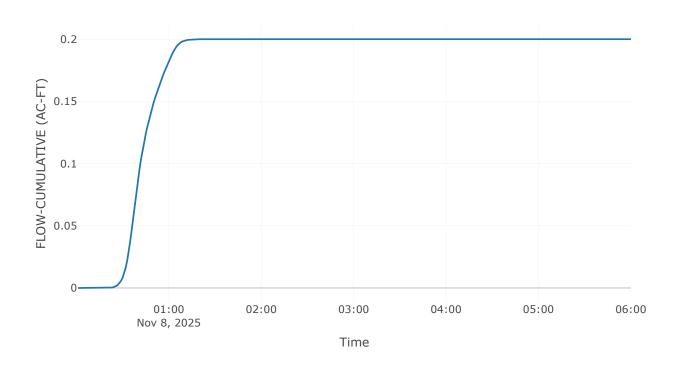
Lag	5
Unitgraph Type	Standard

Results: DA-1

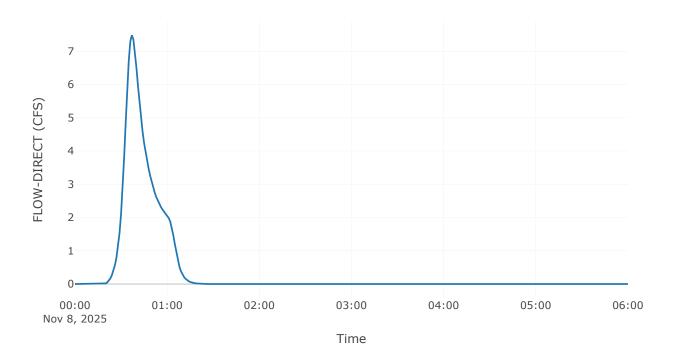
Peak Discharge (CFS)	7.48
Time of Peak Discharge	08Nov2025, 00:37
Volume (IN)	1.92
Precipitation Volume (AC - FT)	0.44
Loss Volume (AC - FT)	0.24
Excess Volume (AC - FT)	0.2
Direct Runoff Volume (AC - FT)	0.2
Baseflow Volume (AC - FT)	O

Precipitation and Outflow





Direct Runoff

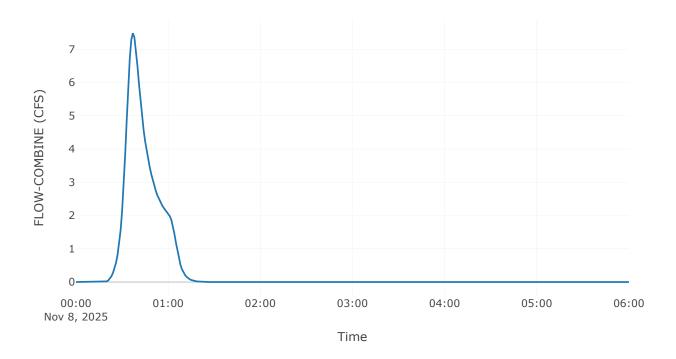


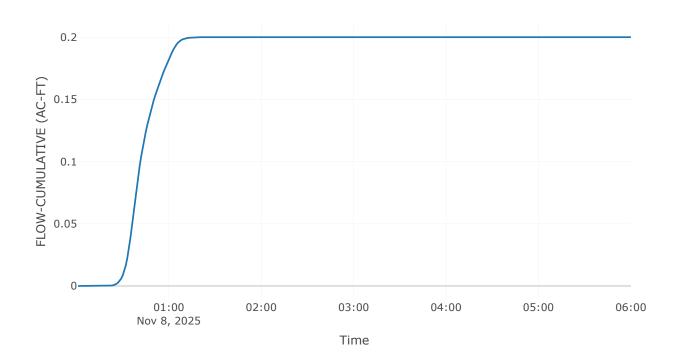
Junction: Creekı

Results: Creeki

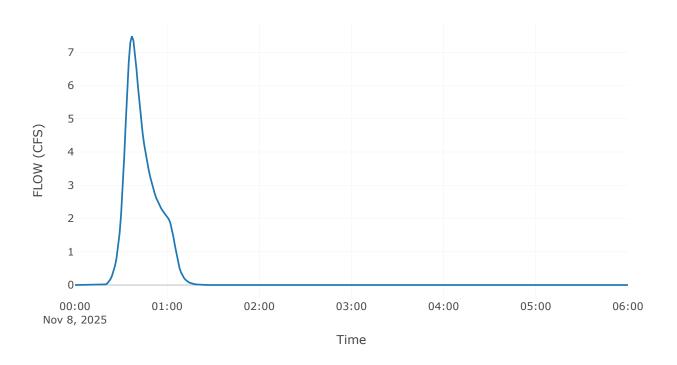
Peak Discharge (CFS)	7.48
Time of Peak Discharge	08Nov2025, 00:37
Volume (IN)	1.92

Combined Inflow





Outflow



Subbasin: DA-2

Area (MI2):0

Downstream : Creek2

Loss Rate: Scs

Percent Impervious Area	O
Curve Number	76

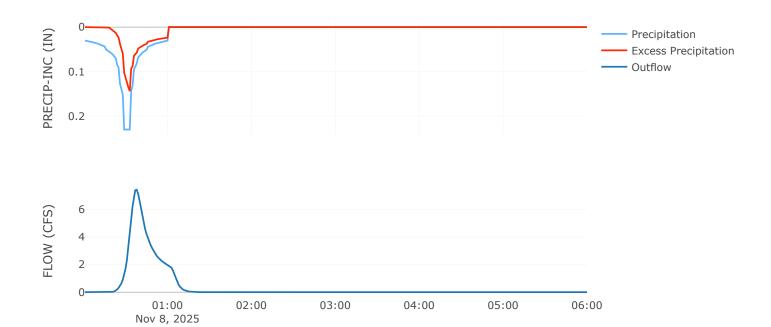
Transform: Scs

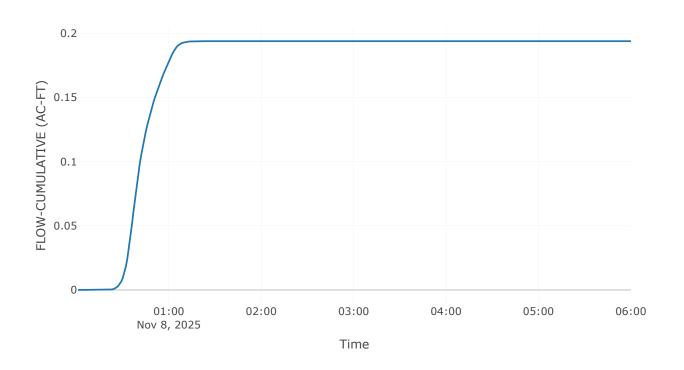
Lag	4.6
Unitgraph Type	Standard

Results: DA-2

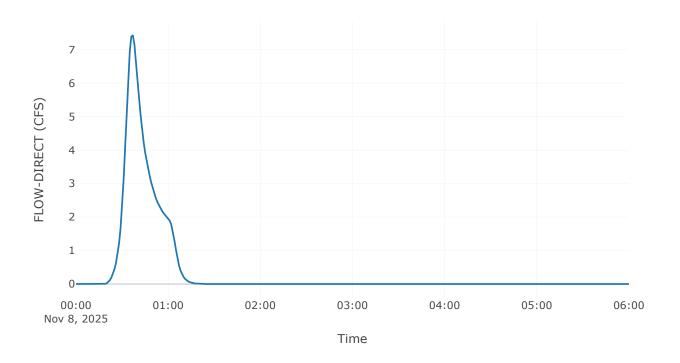
Peak Discharge (CFS)	7.43
Time of Peak Discharge	08Nov2025, 00:37
Volume (IN)	I.92
Precipitation Volume (AC - FT)	0.43
Loss Volume (AC - FT)	0.23
Excess Volume (AC - FT)	0.19
Direct Runoff Volume (AC - FT)	0.19
Baseflow Volume (AC - FT)	O

Precipitation and Outflow





Direct Runoff

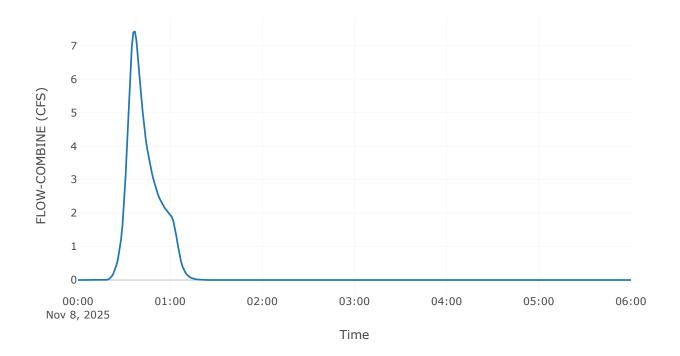


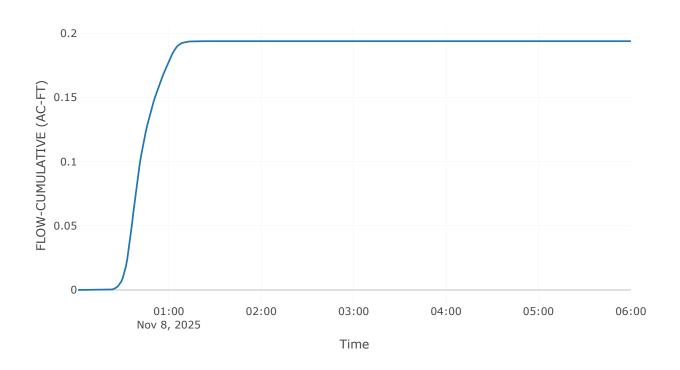
Junction: Creek2

Results: Creek2

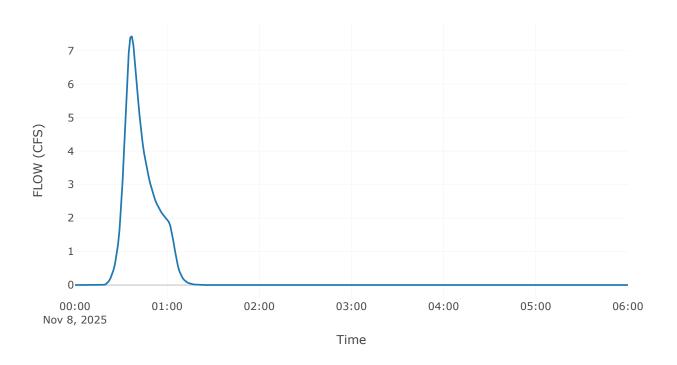
Peak Discharge (CFS)	7.43
Time of Peak Discharge	08Nov2025, 00:37
Volume (IN)	1.92

Combined Inflow





Outflow





Appendix F – Time of Concentration

Existing Conditions Time of Concentration Computations

SubBasin	Flow Type	Surface Condition	Surface Coefficient	US Elev (ft)	DS Elev (ft)	Length (ft)	Slope (ft/ft)	V (fps)	Tt (min)	Tsc (min)	Tch (min)	Σ Tt (min)	0.6Tc
DA-1	Sheet	Short Grass Prairie	0.15	809.83	807.83	100	0.020	0.21	7.85			7.85	
	Shallow	Grassed Waterways	16.13	807.83	780.77	197	0.137	5.98		0.55		0.55	
												8.40	5.04
DA-2	Sheet	Short Grass Prairie	0.15	808.44	804.72	100	0.037	0.27	6.13			6.13	
	Shallow	Grassed Waterways	16.13	804.72	779.38	393	0.064	4.10		1.60		1.60	
												7.73	4.64
DA-3A	Sheet	Short Grass Prairie	0.15	812.43	810.03	100	0.024	0.23	7.30			7.30	
	Shallow	Grassed Waterways	16.13	810.03	794.21	679	0.023	2.46		4.60		4.60	
												11.90	7.14
DA-3B	Sheet	Short Grass Prairie	0.15	794.21	789.04	100	0.052	0.31	5.37			5.37	
	Channel	Natural	0.04	789.04	763.86	270	0.093	5.43			0.41	0.41	
												5.78	3.47

Notes:

⁻P2 = 3.96 inches based on precipitation area zone (PA) 3

⁻Channel velocities calculated using Manning's equation and assuming full bank flow

Proposed Conditions Time of Concentration Computations

SubBasin	Flow Type	Surface Condition	Surface Coefficient	US Elev (ft)	DS Elev (ft)	Length (ft)	Slope (ft/ft)	V (fps)	Tt (min)	Tsc (min)	Tch (min)	Σ Tt (min)
DA-1	Sheet	Short Grass Prairie	0.15	809.83	807.83	100	0.020	0.21	7.85			7.85
	Shallow	Grassed Waterways	16.13	807.83	780.77	197	0.137	5.98		0.55		0.55
												8.40
DA-2	Sheet	Short Grass Prairie	0.15	808.44	804.72	100	0.037	0.27	6.13			6.13
	Shallow	Grassed Waterways	16.13	804.72	779.38	393	0.064	4.10		1.60		1.60
												7.73
DA-3A	Sheet	Short Grass Prairie	0.15	812.43	810.03	100	0.024	0.23	7.30			7.30
	Channel	Bermuda Grass	0.41	810.03	797.00	535	0.024	5.38			0.80	0.80
												8.10
DA-3B	Sheet	Short Grass Prairie	0.15	794.21	789.04	100	0.052	0.31	5.37			5.37
	Channel	Natural	0.04	789.04	763.86	270	0.093	5.43			0.41	0.41
												5.78

Notes:

⁻P2 = 3.96 inches based on precipitation area zone (PA) 3

⁻Channel velocities calculated using Manning's equation and assuming full bank flow



Appendix G – Utilities Calculations

LEON VALLEY BAPTIST CHURCH - RECREATIONAL CENTER



FN042-4 REV A 6/19

San Antonio Water System Infrastructure Planning Equivalent Dwelling Unit (EDU) Calculation Sheet

Subdivision Name: LEON VALLEY	Plat I.D.:	# 18086-006-0620
The estimated Average Sewer Flows or Equivalent Dwelling Ur Plat Review has been calculated by one of the following metho	its that are shown on the SAWS Infrastructure Planning App ds:	lication for Subdivision
Equivalent Dwelling Units (EDU) calculation sheet.		
	imilar facilities based on twelve month data also submitted fo	r review.
 Calculate estimated sewer discharge utilizing accepted S Unknown land use will be calculated at four (4) EDU's pe 		
SAWS has established recommended guidelines to be emplo		to the referenced facility. The
numbers shown, for each type of development, are based o Practice, EPA Technology Transfer Manuals, Uniform Plumbi	yed for ruture discribing calculations which are shown hext in flow rate table measurements from TCEQ regulations, A ing Code fixture unit count and other Wastewater Engineerin	SCE Manuals on Engineering texts. All applicants will use
these guidelines to calculate average daily flows or EDU's.	I doublement which is derived through an anainsaving str	idy of actual measured soun
SAWS will accept sewage flow calculations for any proposed flows for similar facilities in lieu of the above criteria to determ undersigned acknowledges that these EDU calculations repres	ent the intended use of the plat.	
Types of Development: Identify all types of development for each to calculate as Estimated Average Daily Flow (EA day as average sewage flow and 290 gallons per day for av	that will be part of the proposed project and complete t DF) or Equivalent Dwelling Units (EDU's). Note: One (1) erage water flow. (Circle type of units used - EADF or El	he related information listed EDU equals 200 gallons per DU's)
Single Family Homes (1 EDU/Lot) [] Manufactured Homes		EADF or EDU's
Apartments [] Duplexes [] Town Homes [] Condomi		EADF or EDU's
Schools: Elementary [] (5 gal/student) [] Middle (8 gal/stu	dent) [] High School (10 gal/student) [] University/Colleg	e/Other (10gal/student)
Number of Students Number of Faculty & Staff		EADF or EDU's
Hotel [] (100 gal/room) Motel [] (50 gal/room) Number of	Rooms Number of Staff Swimming Pool	EADF or EDU's
Hospital (250 gal/bed) [] Nursing Home (100 gal/bed) []	other Number of Beds Number of Staff	EADF or EDU's
Commercial [] Industrial [] TBDBE Type of Product		ed
Number of Employees Number of Fixtures		EADF or EDU's
(Contact SAWS Wastewater Compliance Division	if a portion of the flow is industrial wastewater. Phone 2	233-3557)
Office Building [] (0.035 gal/sf) Building Square Footage _	Number of employees	EADF or EDU's
Storage [] Climate Control (1 EDU) [] Office Space less th	an 2.500 Sq. Ft. (1 EDU)	EADF or EDU's
Warehouse Building Office Space Sq. Ft(0.07		
Number of Employees (25 gal/employee)		EADF or EDU's
Medical Building [] (0.15 gal/sf) Building Square Footage	Number of employees	EADF or EDU's
Restaurant [] Cafeteria [] (20 gal/seat) Number of Seat		EADF or EDU's
Fast Food [] (5 EDU's per facility) Type of Food Served		EADF or EDU's
Health Club [] Recreational Facility [X] TBDBE Buildin	ng Square Footage 26, 250 Customers per day 525	
Swimming Pool Size Seats in Snack Bar N		EADFor EDU's 7875
Department Store/Retail Store (0.07 gal/sf) Type of Store		ers (5gpd/oustomer)
Number of Employees (25 gpd/employee) Number of		EADF or EDU's
Grocery Store [] Food Store [] Convenience Stores [
Business Hours Number of Customer Fuel Servi		EADF or EDU's
Laundries Number of Machines (200 gal/machine) Bus		EADF or EDU's
Churches [] Auditoriums [] Seating Capacity (5 gr Car Wash [] TBDBE [] Number of Bays (1.5 EDU		EADF or EDU's
Automated Car Wash [] TBDBE Gal per wash		
(Specifications Required)	Number cars p	EADF or EDU's
Service stations []1 EDU Gas Station []2 EDU's Groce	ny/Takeout Food [] 15 EDU's Car Wash	EADF or EDU's
Theatre (1.5 gal/seat) Number of seats Number		EADF or EDU's
	Building Square Footage Number of Er	mployees
Number of Customers Number of seats N		EADF or EDU's
Calculation work space: (Please type or print in ink). Calcuif other form of calculation not shown on this s		Professional Engineer
26,250 Sf - 50 St/person = 525 person	alday => IBC table 1004	1.5
(15 gpd/person) (=25 people) = 7875 jpd	ASSIGNS SOSF/PERSO	M
7875 + 200 = 39.4 & 40 EDU		
⇒ 6" Sewer Latin	TCEQ Chapter	217 8 21732
		.
	Assigns 15 gpd/pers	ον. · · · · · · · · · ·
Additional Information:		
If additional space is needed add a separate sheet, on letter		s form must be completely
filled out and submitted with an original signature. No other	r form will be accepted.	
	OCT 30 1075	
Applicant or Applicant's Agent Signature	OCT 30 2025 Date	



FIRE LINE SIZING:

- > IFC Appendix B + NFPA 24
- => A single 6" is minimum Sizing unless flow is under 1000 grm.
- → Building 15 26250 SF -> 1500 gpm @ 20 psi (IFC BIOS.1)

6" FIRE LINE IS CORRECT & MINIMUM SIZE

DOMESTIC SERVICE · IPC TABLE E103.5(2) & E103.3 (5) ·TCEQ § 290.44 (d) requires minimum 20 psi at all fixtures under peak flow. > IPC TABLE E103.3 (2) 6(3) 10 tolles x 10 FU = 100 FU 10 lavs x 2 FU = 20 FU 8 Showers x 4 FU = 32 FU FUTOTAL = 151 WSFU Per IPC TABLE 152 FU → Q . 55-60 9PM > Q . 57 9PM A) 1" Domestic 57,75 "4015 psi loss B) 1.5" Domestic 1.0 57 1.85 W. - 4.52 (670) 50 185 (1.610 477) = 49.72 ps. loss C) 2" Domestic 1" Domestic ht = 4.52 (670) 57.85 (2.067.87) = 14.73 ps. loss 06.00 SIZE FLOW (gpm) length (11) Head loss (Psi) 400.5 PSI 670 2" DOMESTIC 49.77 61 670 14.73 851 670



IRRIGATION SERVICE

· SAWS IRRIGATION DESIGN QUIDANCE: Limit velocity = 5 Ft/s

· TCEQ § 290.44 (d): system must maintain ≥ 20 psi @ all

· PIPE length to site : ~ 670 ft

· Q=60 as conservative design flow.

hf = 4.52.L. Q1.85

Nominal	10(11)
1.5"	1.610 "
2.0"	2.067"

bo gpm was selected based on manufacturer specifications for commercial rotor irvigation heads, which typically operate @ 2-3 gpm per head, with 18-24 heads per zone, resulting in peak flow of 45-60 gpm.

equipment.

A) 1.8° irrigation line

$$hf = 4.52(670) \cdot \frac{60^{1.85}}{160^{1.85}(1.610^{4.87})} = 20.8 \text{ psi loss}$$

b) 2" irrigation line $ht = 4.52 (670) \cdot \frac{2153}{150^{1.85} (2.067^{4.87})} = 5.3 \text{ psi} \ loss$

2" irrigation line

$$\begin{cases} V = \frac{0.321(60)}{1.610^2} = 7.43 \text{ ft/s} \\ Fail \end{cases}$$

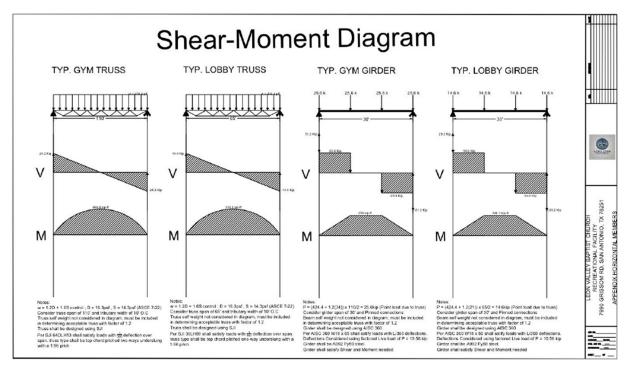
$$V = \frac{0.321 (60)}{2.067^2} = 4.5 \text{ ft/s}$$

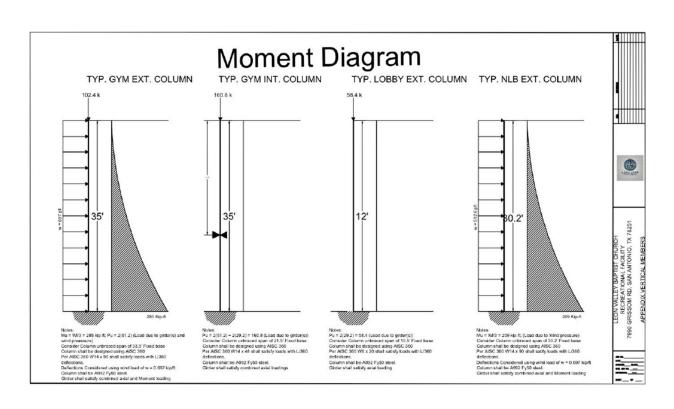
$$0 \text{ hV}$$



Appendix H – Shear Moment diagrams









Appendix I – Structural Design Calculations



STEEL MEMBERS

Determine Load Combinations (2.3.1):

Gym roof Load: **NOT INCLUDING SELF WEIGHT

 $1.4D = 22.82psf; 1.2D + 0.5Lr = 25.56psf; 1.2D + 1.6Lr + 0.5W = 26.21psf \\ 1.4D = 22.82psf; 1.2D + 0.5Lr = 25.56psf; 1.2D + 1.6Lr + 0.5W = 26.21psf$

1.2D+1.6S=42.44 (control)

Lobby roof Load: **NOT INCLUDING SELF WEIGHT

1.4D=22.82psf; 1.2D+0.5Lr=25.56psf; 1.2D+1.6Lr+0.5W=28.06psf 1.4D=22.82psf; 1.2D+0.5Lr=25.56psf; 1.2D+1.6Lr+0.5W=28.06psf

1.2D+1.6S=42.44(control)

TRUSSES

- GYM JOIST
 - Top chord pitched two-ways underslung Pitch 1:96, 64DLH13
 - Design capability = 497.7 plf, unfactored Live roof = 120plf; self-weight 34 plf
 - Mu = 668.5 + 1.2(.034) (110)^2/8 = 730.2 kip-ft
 - o purlins shall run perpendicular at 5' on center.
 - DESIGN BRACING
- LOBBY JOIST
 - Top chord pitched one-way underslung Pitch 1:96, 36LH09
 - Design capability = 499 plf, unfactored Live roof = 120plf; self weight 21 plf
 - Mu = 224.1 + 1.2(.021)(65)^2/8 = 237.4 kip-ft
 - o purlins shall run perpendicular at 5' on center.
 - DESIGN BRACING

GRIDERS ($\phi = 0.9$) (A992)

- GYM 1st Attempt
 - TRY W18 x 65 (A992 Gr50) (Z_x = 133, S_x = 117)

$$\circ \ \ M_u = 256 + \frac{1.2(0.065)\left(30^2\right)}{8} = 265 \, kip - ft$$

$$\phi M_n = 0.9(50)(133) = 498 \, kip - ft$$

o
$$L_b = 30' > L_r = 18.8' > L_p = 5.97' \text{ CHECK}$$

o
$$\phi M_n = \phi M_r = \phi F_{cr} S_x = 182 \, kip - ft \, NG$$



$$\circ \quad F_{cr} = \frac{c_b \pi^2 E}{\left(\frac{L_b}{r_{re}}\right)^2} \sqrt{\left(1 + 0.078 \left(\frac{J_c}{S_x h_o}\right) \left(\frac{L_b}{r_{ts}}\right)^2\right)} = 18.7 \text{ ksi}$$

o
$$\frac{b}{2t_f} = 5.06 < 0.38 \sqrt{\left(\frac{E}{F_y}\right)}; \ \frac{h}{t_w} = 35.7 < 3.76 \sqrt{\left(\frac{E}{F_y}\right)}$$

o
$$\phi V_n = \phi F_v A_w C_{v1} = (1)(50)(18.4)(0.45)(1) = 414 \, kip \, \text{GO}$$

o
$$I_x = 1070 in^4$$
; $\Delta_{max} = \frac{L}{360} \Rightarrow I_{req} = \frac{23Pl^3}{684E\Delta} = 571 in^4 GO$

Gym 2nd Attempt

o Try W18 x 65 With a Kicker Bracing

o
$$L_b = 20' > L_r = 18.8' > L_p = 5.97'$$

$$\circ \quad F_{cr} = \frac{c_b \pi^2 E}{\left(\frac{L_b}{r_{ts}}\right)^2} \sqrt{\left(1 + 0.078 \left(\frac{J_c}{S_x h_o}\right) \left(\frac{L_b}{r_{ts}}\right)^2\right)} = 36.3 \text{ ksi}$$

$$\phi M_n = \phi M_r = \phi F_{cr} S_x = 318.8 \, kip - ft \, GO$$

- Shear and Deflections still satisfied
- MUST DESIGN KICKER BRACES

LOBBY

$$0 \quad M_u = 146.1 + \frac{1.2(0.05)(30^2)}{8} = 153 \, kip - ft$$

$$\phi M_n = 0.9(50)(101) = 378 \, kip - ft$$

o
$$L_b = 30' > L_r = 16.9' > L_p = 5.83' \text{ CHECK}$$

o
$$F_{cr} = \frac{c_b \pi^2 E}{\left(\frac{L_b}{r_{ss}}\right)^2} \sqrt{\left(1 + 0.078 \left(\frac{J_c}{S_x h_o}\right) \left(\frac{L_b}{r_{ts}}\right)^2\right)} = 17.2 \text{ ksi}$$

$$\circ \quad \phi M_n = \phi M_r = \phi F_{cr} S_x = 114 \, kip - ft \, NG$$

LOBBY 2nd Attempt

o
$$L_b = 20' > L_r = 16.9' > L_p = 5.83' \text{ CHECK}$$

$$\circ \quad F_{cr} = \frac{c_b \pi^2 E}{\left(\frac{L_b}{r_{ts}}\right)^2} \sqrt{\left(1 + 0.078 \left(\frac{J_c}{S_x h_o}\right) \left(\frac{L_b}{r_{ts}}\right)^2\right)} = 30.6 \, ksi$$

$$\circ \quad \phi M_n = \phi M_r = \phi F_{cr} S_x = 204.4 \ kip - ft \ \text{GO}$$

o
$$\frac{b}{2t_f} = 6.57 < 0.38 \sqrt{\left(\frac{E}{F_y}\right)}; \frac{h}{t_w} = 45.2 < 3.76 \sqrt{\left(\frac{E}{F_y}\right)} \text{GO}$$

o
$$\phi V_n = \phi F_y A_w C_{v1} = (1)(50)(18.0)(0.355)(1) = 319.5 \, kip$$
 GO

o
$$I_x = 800 \ in^4$$
; $\Delta_{max} = \frac{L}{360} \Rightarrow I_{req} = \frac{23P \ l^8}{684E\Delta} = 572 \ in^4 \ GO$

MUST DESIGN KICKER BRACES



COLUMNS (\phi = 0.9) (A992)

- Exterior GYM Cross-section
 - o TRY W14 x 90

$$\circ \quad \frac{b}{2t_f} = 10.2 < 1\sqrt{\left(\frac{E}{F_y}\right)}; \ \frac{h}{t_w} = 25.9 < 3.76\sqrt{\left(\frac{E}{F_y}\right)} \, \text{NONCOMPACT}$$

o Strong axis:
$$\left(\frac{KL}{r_0}\right) = \frac{33.5(12)}{6.14} = 65.5$$

• Weak axis:
$$\left(\frac{KL}{r_v}\right) = \frac{33.5(12)}{3.70} = 108.6 \text{ CONTROL}$$

o
$$\lambda_c = \pi \sqrt{\left(\frac{2E}{F_v}\right)} = 107$$
; $F_e = \frac{\pi^2 E}{108.6^2}$; $F_{cr} = 0.877 F_e = 21 \, ksi$

o
$$\phi P_n = \phi F_{cr} A = 507 \, kip; \, \frac{P_u}{\phi P_n} = 0.2 \, \text{GO}$$

$$\circ \quad \phi M_p = \phi F_y Z_x = 0.9(50)(157) = 589 \ kip - ft = \phi M_p$$

o
$$\frac{M_u}{\phi M_n} = 0.5$$
; $\frac{P_n}{\phi P_n} + \frac{8}{9} \frac{M_u}{\phi M_n} < 1.0 \text{ GO}$

o
$$\phi V_n = \phi 0.6 F_v t_w d = (0.9)(0.6)(50)(14)(0.44) = 166.3 kip GO$$

- Exterior GYM Cross Section 2nd
 - o TRY W14 x 82

$$\circ \ \ \frac{b}{2t_f} = 5.92 < 0.38 \sqrt{\left(\frac{E}{F_y}\right)}; \ \frac{h}{t_w} = 22.4 < 3.76 \sqrt{\left(\frac{E}{F_y}\right)} \text{COMPACT}$$

o Strong axis:
$$\left(\frac{KL}{r_x}\right) = \frac{33.5(12)}{6.05} = 66.4$$

• Weak axis:
$$\left(\frac{KL}{r_y}\right) = \frac{33.5(12)}{2.48} = 162.1 \text{ CONTROL}$$

o
$$F_e = \frac{\pi^2 E}{162.1^2}$$
; $F_{cr} = 0.877 F_e = 9.55 \, ksi$

$$\circ \quad \phi P_n = \phi F_{cr} A = 206 \, kip; \, \frac{P_u}{\phi P_n} = 0.5$$

$$\circ \quad \phi M_p = \phi F_y Z_x = 0.9(50)(139) = 521 \, kip - ft \, = \, \phi M_p$$

$$\circ \ \ \, \frac{\mathit{M_{u}}}{\mathit{\phi M_{n}}} = 0.55; \,\, \frac{\mathit{P_{n}}}{\mathit{\phi P_{n}}} + \frac{8}{9} \frac{\mathit{M_{u}}}{\mathit{\phi M_{n}}} = 0.99 < 1.0 \, \mathsf{TOO} \, \mathsf{CLOSE}$$

- Exterior Lobby Cross-section
 - o TRY W6 x 16 (A = 4.74 ry = 0.967 Lb=10.5')

$$0 \quad \frac{KL}{r_v} = \frac{(10.5)(12)}{0.967} = 130.3$$

o
$$F_e = \frac{\pi^2 E}{130.3^2}$$
; $F_{cr} = 0.877 F_e = 14.7 \text{ ksi}$

o
$$\phi P_n = \phi F_{cr} A = 63.0 \ kip; \ \frac{P_u}{\phi P_n} = 0.93 \ \text{CLOSE}$$

- Use since W6 x 20 is overdesigned, and columns are supported by standard framing to assist in loading.
- Interior Gym/Lobby Cross- section



$$o \quad \frac{\mathit{KL}}{\mathit{r_y}} = \frac{(21.5)(12)}{1.92} = 131.6; \ \frac{\mathit{KL}}{\mathit{r}} > 4.71 \sqrt{\left(\frac{\mathit{E}}{\mathit{F_y}}\right)}$$

o
$$F_e = \frac{\pi^2 E}{135.1^2}$$
; $F_{cr} = 0.877 F_e = 14.4 \, ksi$

o
$$\phi P_n = \phi F_{cr} A = 190.3 \ kip; \ \frac{P_u}{\phi P_n} = 0.84 \ \text{OK}$$

Non-Loadbearing Exterior Cross-section

o
$$M_u = \frac{Wl}{3} = 209.3 \, kip - ft$$

$$\circ \quad M_u < \phi M_n = \phi F_y Z_x \rightarrow Z_{x,req} = \frac{M_u}{\phi F_y} = 55.82 \ in^3$$

o
$$\phi M_n = \phi F_y Z_x = 230.6 \, kip - ft; \, \frac{M_u}{\phi M_n} = 0.91 \, \text{OK}$$

o Can also use W14 x 43 if too close

$$\circ \quad I_x = 385 \ in^4; \ \Delta_{max} = \frac{L}{360} = 1 \ \Rightarrow \ I_{req} = \frac{w \ t^4}{8E\Delta}$$

o
$$\phi V_n = \phi 0.6 F_v t_w d = (0.9)(0.6)(50)(0.31)(14.1) = 118 kip GO$$

Non-Loadbearing Interior Cross-section

o
$$M_u = \frac{Wl}{3} = \frac{.110(35^2)}{3} = 45 \, kip - ft$$

o
$$M_u < \phi M_n = \phi F_v Z_x = 63.75 \, kip - ft$$

o
$$\phi V_n = \phi 0.6 F_v t_w d = (0.9)(0.6)(50)(8.14)(0.23) = 50.5 \, kip \, GO$$

$$\circ \quad I_x = 61.9 \ in^4; \ \Delta_{max} = \frac{L}{360} = 1 \ \Rightarrow \ I_{req} = \frac{w \ l^4}{8E\Delta}$$

BRACING ($\phi = 0.9$)

GYM TRUSS BRACES

o
$$C = \frac{M_u}{d} = \frac{730.2}{5.33} = 136.9 \text{ kip}; F = 0.02C = 2.74 \text{ kip (TOP)}$$

o
$$C = \frac{M_u}{d} = \frac{0.344(110^2)}{(8)5.33} = 97.6 \text{ kip}; F = 0.02C = 1.95 \text{ kip (BTM - uplift)}$$

- o Top bracing satisfied using perlins
- BTM use L1 ½ x 1 ½ x 1/8 with 22' spacing
- Every 4 joists between .4L and .6L add diagonal brace of same angle size

LOBBY TRUSS BRACES

o
$$C = \frac{M_u}{d} = \frac{237}{5.33} = 79 \text{ kip}; F = 0.02C = 1.58 \text{ kip (TOP)}$$

o
$$C = \frac{M_u}{d} = \frac{0.293 (65^2)}{(8)3} = 51.6 \, kip; F = 0.02C = 1.03 \, kip \, (BTM - uplift)$$

- Top bracing satisfied using purlins
- BTM use L1 ½ x 1 ½ x 1/8 with 16'3" spacing



Every 4 joists between .25L and .5L add diagonal brace of same angle size

GYM GIRDER BRACING

$$C = \frac{M_u}{\frac{d}{2}} = \frac{265(12)}{\frac{18.4}{2}} = 345.7; F = \frac{0.02C}{\sin 45} = 9.8 \, kip$$

$$C = \frac{KL}{\frac{d}{2}} = \frac{(7.1)(12)}{0.764} = 111.5$$

$$F_e = \frac{\pi^2 E}{111.5^2}; F_{cr} = \left(0.658 \frac{F_y}{F_e}\right) F_y = 18.7 \, ksi$$

$$\phi P_n = \phi F_{cr} A = 20.0 \, kip; \, \frac{P_u}{\phi P_n} = 0.49 \, \text{OK}$$

LOBBY GIRDER BRACING

$$C = \frac{M_u}{\frac{d}{2}} = \frac{153(12)}{\frac{17.7}{2}} = 207.5; F = \frac{0.02C}{\sin 45} = 5.9 \ kip$$

$$C = \frac{KL}{\frac{d}{2}} = \frac{(7.1)(12)}{\frac{10.605}{2}} = 140.3$$

$$F_e = \frac{\pi^2 E}{140.3^2}; F_{cr} = 0.877 F_e = 12.7 \ ksi$$

$$\phi P_n = \phi F_{cr} A = 10.8 \ kip; \ \frac{P_u}{\phi P_n} = 0.54 \ \text{OK}$$

$$\text{OUSE L2 X 2 X 1/4}$$

Purlins

0
$$w = 42.4(5) = 212plf; M = \frac{0.212(10^2)}{8} = 2.65 kip - ft$$

0 $\phi M_n = \frac{\phi F_y Z_x}{12} = \frac{0.9(36)(2.29)}{12} = 6.2 kip - ft$
0 $R_u = \frac{wl}{2} = \frac{.212(10)}{2} = 1.06k$

Wall Girt (30' spacing)

$$\begin{array}{l} \circ \quad w = 23.5(5) = 116.5plf; \ M = \frac{0.1165(30^2)}{8} = 13.1 \ kip - ft \\ \circ \quad \phi M_n = \frac{\phi F_y Z_x}{12} = \frac{00.9(36)(9.63)}{12} = 36.1 \ kip - ft \\ \circ \quad R_u = \frac{wl}{2}; \ \Delta_{max} = \frac{5w \ l^4}{384El} \\ \circ \quad \text{Use C8 x 11.5} \end{array}$$

Wall Girt (22' spacing EXT.)

$$\begin{array}{l} \circ \quad w = 23.5(5) = 116.5plf; \ M = \frac{0.1165(22^2)}{8} = 7.05 \ kip - ft \\ \circ \quad \phi M_n = \frac{\phi F_y Z_x}{12} = \frac{0.9(36)(6.18)}{12} = 23.2 \ kip - ft \\ \circ \quad R_u = \frac{wl}{2}; \ \Delta_{max} = \frac{5w \ l^4}{384El} \\ \circ \quad \text{Use C6} \times 10.5 \end{array}$$



o
$$w = 5(5) = 25plf$$
; $M = \frac{0.0.025(22^2)}{8} = 1.51 \, kip - ft$
o $\phi M_n = \frac{\phi F_y Z_x}{12} = \frac{0.9(36)(2.29)}{12} = 6.2 \, kip - ft$
o $R_n = \frac{wl}{12}$; $\Delta_{max} = \frac{5w \, l^4}{12}$

$$\circ \quad R_u = \frac{wl}{2}; \ \Delta_{max} = \frac{5w \, l^4}{384EI}$$

Connections (for connections most cases $\phi = 0.75$)

PL - A572 Gr50; L - A36

PURLINS CONNECTION

- Use L2 x L2 x 3/16 angle clip
- o Use 1 1/2" dia A325 bolt to purlin
- Use 3/16 fillet weld 2"min on both sides to joist

o BOLT -
$$\phi R_n = \phi 0.48 F_u A_b = 0.75(0.48)(120)(.196) = 8.5k$$
 OK

o Bearing -
$$\phi R_n = \phi 1.2 L_c t F_u \rightarrow web = 16.1k$$
; angle = 16.4k

o WELD
$$-t_w = 0.133$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 4.16 k x^2 = 8.3 k$ OK

GYM TRUSS-GIRDER CONNECTION

$$\circ \quad R_u = \frac{.4244(110)}{2} + \frac{1.2(0.034)(110)}{2} = 25.6k$$

$$\phi P_n = \phi F_v A_a = 64.8 \times 2 = 129.6k$$

$$\phi P_n = \phi F_u A_s = 71.9 \times 2 = 143.8k$$

- Use ¼ fillet weld 6" on leg to girder seat
- Use ¼ fillet weld 6" on leg to truss

o
$$t_w = 0.177$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 33.4 k$

- Use PL ¾ x 14" x 14" with ¼ fillet perimeter weld for girder seat and column
- *for the W12x50 column use PL ¾ x 12" x 12" instead

LOBBY TRUSS-GRIDER CONNECTION

$$\circ \quad R_u = \frac{.4244(65)}{2} + \frac{1.2(0.021)(65)}{2} = 14.6k$$

Use 2 – L3 x 3 x ¼ 6" long angles

$$\phi P_n = \phi F_N A_a = 64.8 \times 2 = 129.6k$$

$$\phi P_n = \phi F_u A_s = 71.9 \times 2 = 143.8k$$

- o Use 1/4 fillet weld 6" on leg to girder seat
- Use ¼ fillet weld 6" on leg to truss

o
$$t_w = 0.177$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 33.4 k$

Use PL ¾ x 7" x 7" with ¼ fillet perimeter weld for girder seat and column cap



 For connecting to column create seat plate use PL ¾" x 8" x 6" and have two angles under for support with 3/16 fillet perimeter weld

TRUSS BRACING CONNECTION

- Weld PL 3/16" x 3" x 4" to truss bottom chord with 3/16" fillet weld 2" min on both sides
- o $t_w = 0.133$; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 8.3 k \times 2 = 16.7 k min$
- Use 1 ½" A325 bolt to connect brace to gusset
- o BOLT $\phi R_n = \phi 0.48 F_n A_n = 0.75(0.48)(120)(.196) = 8.5k$

GYM GIRDER BRACING CONNECTION

- Weld PL 3/8 X 6" X 8" gusset plate to both webs
- o Weld with 3/16 fillet weld 8" on both sides

o
$$t_w = 0.133$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 33.5 k$

- o Use L2 1/2 X 2 1/2 X 1/4
- $\phi P_n = \phi F_v A_a = 53.5k$
- $\phi P_n = \phi F_u A_s = 59.4k$
- o 2-3/4 A325 bolt(s) to connect brace to plates
- o Bolt $\phi R_n = 2 \times 17.9k = 35.8k$

LOBBY GIRDER BRACING CONNECTIONS

- Weld PL 3/8 X 6" X 8" gusset pate to both webs
- o Weld with 3/16 fillet weld 8" on both sides

o
$$t_w = 0.133$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 33.5 k$

- o UseL2X2X1/4
- $\phi P_n = \phi F_v A_a = 44.7k$
- $\phi P_n = \phi F_n A_s = 49.6k$
- o 2-1/2 A325 bolt to connect brace to plates
- $\phi R_n = \phi 0.48 F_u A_b = 0.75(0.48)(120)(.196) \times 2 = 17k$

GYM GIRDER-COLUMN CONNECTION

o
$$R_u = 51.2 + \frac{.065(30)}{2} = 52.2 \, kip$$

- o Try 34 " dia A325 Bolts
- o $n \ge \frac{R_u}{\phi R_n} = \frac{52.2}{35.8} = 1.458 \rightarrow \text{use } 2 \frac{3}{4} \text{ "dia A} = 325 \text{N bolts}$
- o Try PL 3/8" x 10" x 10" (3 bolts, 3" vertical spacing, 2" edge distance)

o
$$V_{u, pl} = \frac{V_u}{2} = 26.1k$$
; $V_{bolt} = \frac{26.1k}{2} = 13.05 k$

o PL -
$$\phi R_n = \phi 1.2 L_c t F_u = \phi 1.2 (1.5) (0.375) (65) = 32.9 \frac{k}{holt} GO$$

o WEB -
$$\phi R_n = \phi 1.2 L_c t F_u = \phi 1.2 (1.5) (0.45) (65) = 39.5 \frac{k}{holt} GO$$

$$\circ \quad \mathsf{PL} - A_{vn} = t_p L_v = 2.25; \ A_{nt} = 0.75; \ \phi R_n = \phi \big(0.6 F_y A_{vn} + F_u A_{nt} \big) = 87.2 \ k \ \mathsf{G}$$

o WEB -
$$A_w=d_wt_w=7.2;~\phi V_n=\phi 0.6F_yA_w=194k~{\rm GO}$$



- o WEB $\phi V n = \phi 0.6 F_u A_w = 211 k \text{ GO}$
- o USE 5/16" FILLET WELD 10" (E70)
- o WELD $t_w = 0.221$; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 69.6 k$ OK
- For W12 x 50 use PL 3/8 x 10" x 7"

LOBBY GIRDER-COLUMN CONNECTION

o
$$R_u = 29.2 + \frac{.035(30)}{2} = 29.8 \, kip$$

o Try 34 " dia A325 Bolts

o
$$n \ge \frac{R_u}{\phi R_n} = \frac{29.9}{35.8} = 0.84 \rightarrow 1 \ but \ use \ 2 - \frac{34}{9} \ " \ dia \ A325 \ N \ bolts$$

o Try PL 3/8" x 6" x 6" (2 bolts, 4" vertical spacing, 2" edge distance)

o
$$V_{u, pl} = \frac{V_u}{2} = 15k$$
; $V_{bolt} = \frac{15k}{2} = 7.5 k$

o PL -
$$\phi R_n = \phi 1.2 L_c t F_u = \phi 1.2 (1.5) (0.375) (65) = 32.9 \frac{k}{holt}$$
 OK

o WEB -
$$\phi R_n = \phi 1.2 L_c t F_u = \phi 1.2 (1.5)(0.3)(65) = 26.3 \frac{k}{bolt} \text{OK}$$

o PL -
$$A_{vn} = t_v L_v = 2.25$$
; $A_{nt} = 0.75$; $\phi R_n = \phi (0.6 F_v A_{vn} + F_u A_{nt}) = 87.2 k G$

o WEB -
$$A_w = d_w t_w = 4.8$$
; $\phi V_n = \phi 0.6 F_v A_w = 129.9 k$ OK

o WEB -
$$\phi V n = \phi 0.6 F_u A_w = 140.8 k \text{ OK}$$

o WELD -
$$t_w = 0.221$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w L_w = 41.8 k \text{ OK}$

WALL GIRT CONNECTION

- Use 2 ¾" dia A325 bolts connect girt web to column flange
- o BOLT $\phi R_n = 2 \times 17.9k = 35.8k$

GYM EXT COLUMN BASE CONNECTION

- Use base plate PL 1 ½" x 30" x 30"
- o 3/8" fillet weld flanges and web both sides

$$\circ \quad q = \frac{p_u}{A_p}; \ w = q b_f; \ M = \frac{w(5)^2}{2} = 10k - in \, per \, in$$

o
$$S = \frac{t^2}{6}$$
; $f_b = \frac{M}{S} = \phi f_y \to t \ge 1.16 \text{ OK}$

o
$$e = \frac{M_u}{P_u} = 33.4in \gg \frac{N}{6}$$
, so base in tension

o Place 2 anchor rods on tension side 2 on compression side

o
$$T = \frac{M_u}{z} = 171k$$
; $T_{rod} = \frac{171}{2} = 85.5$; $for 4 \rightarrow 40.8 k$

o Use 1 1/4" dia anchor rods

$$\phi T_n = \phi 0.9 F_v A_a = 45.6 k \text{ OK}$$

- Add stiffener PL ¾" x 8" x 12" to center of Column web
- o 3/8" Fillet weld 8" to base plate both sides

GYM-LOBBY INT COLUMN BASE CONNECTION



o Use base plate PL 1" x 20" x 20"

$$o \quad q = \frac{P_u}{A_p}; \ t \ge 5\sqrt{\left(\frac{2q}{\phi F_y}\right)} = 0.75 \, \text{OK}$$

Use 4 - ¾" dia Anchor rods

$$\phi T_n = \phi 0.9 F_y A_g = 16.4 k \text{ OK}$$

o 1/4" fillet weld column perimeter to plate

o
$$t_w = 0.177$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w = 5.57 \frac{k}{in}$

LOBBY EXT BASE CONNECTION

Use base plate PL ½" x 16" x 16"

$$o \quad q = \frac{P_u}{A_p}; \ t \ge 3\sqrt{\left(\frac{2q}{\phi F_y}\right)} = 0.4$$

o Use 4 - 5/8" dia Anchor rods

$$\phi T_n = \phi 0.9 F_v A_a = 11.4 k$$

o 14" fillet weld column perimeter to plate

o
$$t_w = 0.177$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w = 5.57 \frac{k}{in}$

NON-LOADBEARING EXT BASE CONNECTION

Use base plate PL 1" x 22" x 22"

$$0 \quad q = \frac{P_u}{A_p}; \ t \ge 6\sqrt{\left(\frac{2q}{\phi F_y}\right)} = 0.9$$

o
$$T = \frac{M_u}{z} = 139.3k$$
; $T_{rod} = \frac{139.3}{4} = 34.8$

o Use 4 - 1 1/4" dia Anchor rods

$$\phi T_n = \phi 0.9 F_y A_g = 45.6 k$$

o 3/8" fillet weld flanges and web both sides

NON-LOADBEARING INT BASE CONNECTION

Use base plate PL 5/8" x 14" x 14"

$$o \quad q = \frac{P_u}{A_v}; \ t \ge 4\sqrt{\left(\frac{2q}{\phi F_v}\right)} = 0.6$$

o
$$T = \frac{M_u}{z} = 40.2k$$
; $T_{rod} = \frac{40.2}{2} = 20.1$

Use 4 – 7/8" dia anchor rods

$$\phi T_n = \phi 0.9 F_y A_g = 22.3 \frac{k}{rod}$$

o 1/4" fillet weld column perimeter to plate

o
$$t_w = 0.177$$
; $\phi R_n = \phi 0.6 F_{EXX} t_w = 5.57 \frac{k}{in}$



Appendix J-TIA Worksheet



			T										
Complete Nile form or an all				mpact Anal					N2753740 1155	110-1-2			
Complete this form as an aid			_	Frame Impact.		_				11th Edi	tion.		
						Worksheet Prepared by: Conrad Montes							
Project Location: 7980 Grissom Road, San Antonio TX									Owner Owner's Agent			Agent	
Email: lonestarengineering@lonestar.com				Address: 1234 UTSA Boulevard Associated Record Type: Zoning MDP					Date:				
Jurisdiction: X COSA I			Other:					Zoning	☐ MDP	☐ Pla	t	Building	g Permit
TIA Record Number (if ap	-):				ted Record							
Proposed Type of Developm					ritical Pea		PM		our Override:	PM			
Land Use		ITE Code	Project Size				r Trip Rate		our Trips (PF	IT)		rates and crit	
Recreational Community C	Center	495	26.25	1,000 SF GF	A	2.5		66		_		ur are autom	
												ulated in this	
												d on the lines	
												1th edition.	
												automatic pe ulator, check	
Previous Development on Si	ite:				ritical Pea				our Override:			ur Override l	
Land Use		ITE Code	Project Size	Unit		Peak Hou	Trip Rate	Peak H	our Trips (PI	IT)		the correct p	
												custom or ac	
												, please use t	
												ge of the wor	
										\neg	pa	ge of the wor	A SHEEL
										\neg	1		
Total Trips: Please ensure	e land use	s for all lots/pa	rcels are inclu	led in the abov	e sections					_			
Proposed Development	Previous	Developme	nt Differen	ce in PHT	I	f there is an i	ncrease of	6 PHT and	an increase of	10% of	the tota	l PHT, a new	TLA is
66			66	100%	\neg				required				
Previous TIA Report (if pro	perty has	a TLA on file)			_								
Proposed Development	Approve	ed TIA PHTs	Differen	ce in PHT	TLA	Number:				ı			
66					TLA	Name:				l			
										•			
*** I	TEMS E	BELOW TH	IS LINE ARI	E FOR OFFI	ICLAL U	SE ONLY.	DO NOT	WRITE	BELOW TH	IS LIN	E. ***		
Turn Lane Requirements fo	r Develo	pments with I	ess than 76 Pl	HT per UDC 3	5-502(e)(2) (F	or more th	n 76 PHT.	this analysis v	vill be in	cluded	in the TIA)	
Right Turn Lanes Require	d 🔲	at			Left Tu	m Lanes Re	quired [at					
□ at													
Comments:													
☐ This deve	lopment i	s located on a	TxDOT roadw	av. TxDOT rev	iew of RC	W and acces	s is require	d. Please st	bmit the plat a	and other	associa	nted	
			OT for review				•						
		_											
☐ A TIA R	eport is	Required.	X A TLA R	eport is Not l	Required						Wor	rksheet Last Update	d 4/1/2024
A TIA U				ation Study is									



Appendix K – Rough Proportionality Worksheet



DEVELOPMENT SERVICES				Roug		Antonio, Texas ality Worksheet		
•						,		
Development Name:	Leon Valley Bay	ptist Recreation	onal Cente	r				
Applicant:	Conrad Montes							
Legal Description (Lot, Block):	18086 BLK 6 LC	T 2 Leon Val	ley Baptist	Church Subd				
Case / Plat Number:				Date:	October 23, 2025			
						Worksheer Lear Updated: 11/15/5004		
DEMAND - Traffic Generated by Proposed Dev	elopment	Peak Period to		AM Peak EPM Peak				
Land Use Type: Development Unit:	Intensity:	Peak Hour Trip	Internal Capture	Trip Langth:	Demand: (vehicle-miss)	Impact of Development: (\$)		
Recreational Community Center 1,000 SF GFA	26.25	Rate: 2.50	Rate: 0%	(miss) 1.50	98.44	\$420.273		
						7.3.3.		
				l .				
This row allows for the entry of unique or uncommon land uses not included within manual entry of the development unit englor trip rate. It shall only be used when (the current ITE Trip G a) sufficient date in eve	eneration; or whe elable to support	o gircumativo so alternative	es require seloulation; and				
(b) It is agreed to by the City during the TIA according meeting.								
IMPACT OF DEMAND PL					98.44	\$420,273		
Estimate	ed Average Co	et Per Vehl	cle-Mile:	\$ 4,269.44				
Roadway Supply- Off-Site Roads to be Built or F	funded by the	Applicant		,				
Roadway Name:	Classification:		Roadway Length:		Supply Cost Estimate: (5)	Cost Estimate : (\$)		
			(Feet)	ı	Esternate: (5)			
	POAD	WAY SLIDE	I V ADDI	I En To even	EM SUBTOTAL:	\$0		
Interrection Improvements Consider Improve	100000				LIN GODIOTAL.	•		
Intersection Improvements - Specific Improver	Description of Im		ed by the	э дрисапт.		Estimated Cost ¹³ : (5)		
						1,00		
INTERSECTION IMPROVEMENTS ADDED TO SYSTEM SUBTOTAL: \$0								
Right-of-Way Dedication - ROW to be dedicated by the Applicant:								
ROW Dedication:	General Descripti		lication:			Estimated Cost ¹¹ : (5)		
					EM SUBTOTAL:	\$0		
TOTAL VALUE OF SUPPLY ADDED TO THOROUGHFARE SYSTEM: \$0								
Notes: *Based on an estimated cost to provide the tradway supply (construction and engineering) based on the classification; *Revised cost estimate, if available, for construction and engineering based on more detailed preliminary engineering and/or design; *Estimated intersection improvement costs; *Cost of digit-of-way should be estimated using Appraisal District values (number of square feet of dedication multiplied by								
the unimproved land values).								
SUPPLY / DEMAND COMPARISON: A comparison of the capacity provided by a development against the traffic impacts of								
SUPPLY/DEMAND COMPARISON. the proposed development.								
TOTAL IMPACT OF DEMAND PLACED ON	THOROUGHEAR	E SYSTEM		20,273	Comparison	I		
TOTAL VALUE OF CAPACITY (SUPPLY) ADDED TO				\$0				
Note: Minimum Standards for eccess to and from a development may supercede the results of this analysis.								
more measurest community for access to and more a development may super-	and the results of th	a arrayan.						



Appendix L – Budget



Engineering Design Fee

	PM &	Structural		Geo & Foun	Util.	Land dev. &	
	Transportation	Engineer	H & H Engineer	Engineer	Engineer	Env.	
Billing Rate per hour	\$125.00	\$100.00	\$90.00	\$95.00	\$90.00	\$80.00	
30% Milestone	\$62,500.00	\$58,600.00	\$36,000.00	\$55,100.00	\$40,050.00	\$32,000.00	
Site Visit and Assesment	80	80	120	100	80	160	
Data Collection and Research	80	136	100	80	60	60	
Structural Design	80	140	0	180	100	0	
Permit Accumulation	60	60	80	60	125	100	
Utility Planning	0	80	100	160	80	80	
Overseeing	200	90	0	0	0	0	
Total Hours	500	586	400	580	445	400	
60 % Milestone	\$65,500.00	\$64,500.00	\$48,600.00	\$47,975.00	\$50,850.00	\$40,000.00	
Comprehensive Grading	0	80	120	0	100	160	
Floor Plan for Facility	0	105	0	105	0	0	
Comprehensive Structural Design	100	100	0	160	100	0	
Fire Safety	0	80	0	80	40	40	
Sewer Design	0	0	80	0	40	40	
Comprehensive Utility	100	60	90	100	80	80	
Pavement Design	0	60	170	0	80	80	
Permit Accumulation	60	80	80	60	125	100	
Overseeing	264	80	0	0	0	0	
Total Hours	524	645	540	505	565	500	
100% Milestone	\$57,875.00	\$58,000.00	\$41,400.00	\$50,350.00	\$48,600.00	\$30,400.00	
Finalized Grading	0	80	100	0	100	160	
Finalized Structural Design	80	120	0	220	120	0	
Finalized Fire plan	0	80	0	80	60	0	
Fianlized Sewer Design	0	0	0	0	60	60	
Finalized Utilities	60	80	100	170	100	100	
Finalized Pavement	0	0	180	0	60	60	
Finalized Permits	60	80	80	60	40	0	
Overseeing	263	140	0	0	0	0	
Total Hours	463	580	460	530	540	380	
Subtotal	\$185,875	\$181,100	\$126,000	\$153,425	\$139,500	\$102,400	



Cost Breakout

Category	Subcategory	Cost (\$)		
Facility Building Cost	Main Building Structure	\$ 3,000,000.00		
Facility Building Cost	Interior Build-Out	\$ 750,000.00		
Facility Building Cost	MEP Systems	\$ 500,000.00		
Construction Materials	Concrete & Rebar	\$ 250,000.00		
Construction Materials	Structural Steel	\$ 225,000.00		
Construction Materials	Roofing & Envelope Materials	\$ 200,000.00		
Construction Materials	Finishes & Fixtures	\$ 208,000.00		
Site Work	Earthwork & Grading	\$ 200,000.00		
Site Work	Paving & Parking	\$ 175,000.00		
Site Work	Utilities (Water/Sewer/Electric)	\$ 125,000.00		
Site Work	Landscaping	\$ 50,000.00		
Structural Components	Foundations	\$ 140,000.00		
Structural Components	Slab-on-Grade	\$ 100,000.00		
Structural Components	Beams/Columns/Girders	\$ 80,000.00		
Misc. Construction Items	General Conditions	\$ 70,000.00		
Misc. Construction Items	Safety & Temporary Facilities	\$ 48,700.00		
Mobilization, Insurance & Bond	Mobilization	\$ 600,000.00		
Mobilization, Insurance & Bond	Insurance & Bonding	\$ 600,000.00		
Construction Contingency	Allowances	\$ 1,280,000.00		
Engineering & Design Fees	Architectural	\$ 388,300.00		
Engineering & Design Fees	Civil/Structural/MEP	\$ 500,000.00		
Testing, Permitting, Admin	Permits	\$ 5,000.00		
Testing, Permitting, Admin	Testing & Inspections	\$ 5,000.00		
	\$ 9,500,000.00			